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## UPGA301A Pulse Circuit Analysis

The dynamic on-state characteristics of the UPGA301A are described. This device is assembled in Microsemi's PowerMITE3® low profile, surface-mount package. The UPGA301A is an E-processed high speed silicon controlled rectifier.

Typical applications for the UPGA301A are current pulse drivers for laser diodes and squib firing circuits. These circuits require high speed switching, low dynamic on-state impedance, signal fidelity, and efficient energy transfer.

In these applications, UPGA301A offers high efficiency for thermal diffusion of heat transfer and excellent electrical characteristic matching to RF circuit boards.

The dynamic on-state characteristics of the UPGA301A are modeled. This allows the circuit designer to accurately access the dynamic device electrical and thermal behaviors in these circuits.

A forward voltage on-state model is generated using typical measured on-state characteristics  $V_T$ , as a function of on-state forward current  $I_T$ .

The on-state model for  $V_T$ , for the UPGA301A was developed from a curve fit of typical test data produced from values of short duration  $I_T$  pulses applied to the UPGA301A. The model is:

$$V_T = A + B \ln(I_T) + C(I_T) + D\sqrt{I_T}$$

*figure 1*

$I_T$ , is the forward on-state current (amperes) and  $V_T$ , is the on-state voltage (volts). The accuracy of the model is tested by comparing calculated values to the measured values and is found to be within one-half percent over the range of current from the micro-ampere range up to the current limit of the device. Note, the model will not work for zero current.

The values of the constants apply specifically to the UPGA301A device. They are listed below:

$$\begin{aligned} A &= 0.8775 \text{ volt} \\ B &= 0.0389 \text{ volt} \\ C &= 0.0503 \text{ volt} \\ D &= 0.0223 \text{ volt} \end{aligned}$$

Junction power dissipation is the product of the applied current  $I_T$ , and the on-state voltage  $V_T$ . The on-state voltage  $V_T$ , responds non-linearly to the applied current  $I_T$ . The instantaneous power is calculated using a piece-wise approach over the time span of the applied current range.

The advantage of using the  $V_T - I_T$  model is in applications where non-repetitive, non-linear current pulses are delivered through the UPGA301A SCR powermite switch.

LED, Laser Diodes, and fusible squibs are applications where current sources resulting from capacitor discharges are passed through the SCR switch into a series connected load.

The model describes the dynamics of the voltage and effects such as internal power dissipation. Device energy may be determined from this. A thermal diffusion model is developed for the UPGA301A using the properties of the semiconductor material, and the specific geometry of the UPGA301A. This model allows the designer to predict the SCR's thermal loading during the application of the power pulse delivered to the load.

UPGA301A is specifically designed for delivering narrow high current pulses. The width of the pulse should be much smaller than the thermal time constant of the silicon die and PowerMITE3 package combination to prevent thermal runaway during high current switching. Examples are shown to illustrate the effects in the accompanying design descriptions. The thermal diffusion model and its derivative developed for the UPGA301A is:

$$T_J(t) = \frac{2P_T(t)}{\sqrt{\pi}} \cdot \frac{1}{K_{\theta_{si}}} \cdot \frac{1}{A_J} \cdot \sqrt{D_{\theta_{si}}t + T_A}$$

figure 2

$$T'_J(t) = 2 \frac{\frac{d}{dt}[P_T(t)]}{\sqrt{\pi} \cdot K_{\theta_{si}} \cdot A_J} \cdot \frac{1}{\sqrt{D_{\theta_{si}} \cdot t}} + \frac{P_T(t)}{\sqrt{\pi} \cdot K_{\theta_{si}} \cdot A_J \cdot \sqrt{D_{\theta_{si}} \cdot t}} \cdot D_{\theta_{si}}$$

figure 2b

$T_J(t)$  is the junction temperature,  $P_T(t)$  is the junction power dissipation, and  $T_A$  the operating ambient temperature.

The material and physical properties of the UPGA301A used in the analysis are:

UPGA301A chip area	$A_C = 2860 \text{ mil}^2$
Active junction area	$A_J = 442 \text{ mil}^2$
chip mass	$M_C = 1.092 \text{ mg}$
Silicon density	$\rho_{si} = 2.33 \text{ gm/cm}^3$
Silicon thermal conductivity	$K_{\theta_{si}} = 1.45 \text{ watt/cm} \cdot \text{C}$
Silicon specific heat	$cp_{si} = 0.7 \text{ watt sec/gm} \cdot \text{C}$
Silicon diffusivity	$D_{\theta_{si}} = 0.9 \text{ cm}^2/\text{sec}$
Chip thermal resistance	$R_{\theta_{si}} = 0.949 \text{ C/watt}$
Chip thermal capacitance	$C_{\theta_{si}} = 7.644 \times 10^{-4} \text{ watt sec/C}$
Chip thermal time constant	$\tau_{\theta_{si}} = 726 \mu\text{s}$

The first example is a half-sinusoidal, non-repetitive pulse applied to the anode of the UPGA301A with a series connected cathode  $1\Omega$  resistive load.

The circuit operates at an ambient temperature  $T_A$ . The half-sine current pulse  $i_T(t)$  is applied to the anode of the UPGA301A. The peak value is 100 amperes. The response of the SCR to the applied current is calculated and illustrated in the accompanying graphs. These are  $P_T(t)$  and junction temperature  $T_J(t)$ .

The current pulse and its derivative is represented by:

$$i(t) = I_{pk} \cdot \sin(a \cdot t)$$

figure 3

$$i'(t) = I_{pk} \cdot \cos(a \cdot t) \cdot a$$

figure 3b

The UPGA301A presents a dynamic resistance to the applied pulse. The dynamic resistance of the SCR is in series with the resistive load. Although the load in our example is pure resistance it may be non-linear as well. In this example the

dynamic resistance is represented and the total circuit resistance by:

$$Z_{SCR}(t) = \frac{v_T(t)}{i_T}, Z = Z_{SCR}(t) + R_{LOAD}$$

figure 4

The period of the applied non-periodic, half-sine pulse is 500ns. The peak current is 100A. The peak forward on-state voltage  $V_T$  is determined from equation (figure 1) by setting  $I_T$  to 100A. The value is 6.32V at the peak current point. The peak thermal junction temperature  $T_J$ , occurs slightly after the peak current point at 148ns. This is the result of the thermal time constant of the UPGA301A. The combined delay  $t_d$ , and rise time  $t_r$ , of the UPGA301A is 50ns maximum. This results in a delay and rise of the response voltage and junction temperature. The calculated peak junction temperature is about  $83^\circ\text{C}$ .

The voltage source required to provide 100 amps peak is determined by multiplying the required peak current times the dynamic resistance  $Z$ . So, for a  $1\Omega$  load the required source voltage to produce the 100 amp peak is 106.32 volts.

The second example illustrates another common application. Capacitor  $C_O$ , the energy storage device, discharges through the SCR switch and a low impedance load. The circuit inductance  $L_O$ , capacitor  $C_O$  with its initial charge voltage  $V_O$ , and the load resistance  $R_L$  are specified. The equation defining the current as a function of time is:

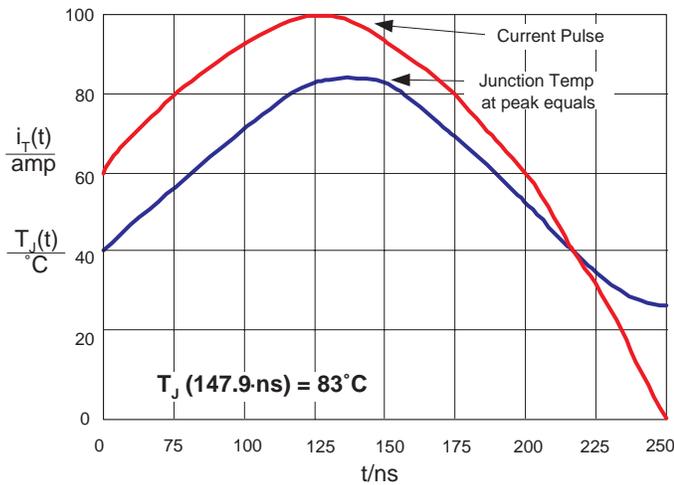
$$i_T(t) = \frac{V_o}{\sqrt{L_o \text{ over } C_o}} \cdot \exp\left[-\frac{Z(t) \cdot t}{2L_o}\right] \cdot \sin\left[\sqrt{\frac{1}{L_o \cdot C_o}} \cdot t\right]$$

figure 5

In this example the current pulse is not sinusoidal and is non-linear. The capacitor charged initially to  $V_O$  delivers current through the dynamic resistance of the SCR and the series connected load. The value  $Z$  is determined as in (4.) above. The components used in this example analysis are  $L_O = 75\text{nH}$ ,  $C_O = 10\mu\text{F}$ , and  $R_L = 1\Omega$ . A peak current of 85.6A occurs at 125ns, SCR  $V_T(\text{pk})$  is 5.57V, and  $T_J(\text{pk})$  is  $72^\circ\text{C}$  at 215.6ns.

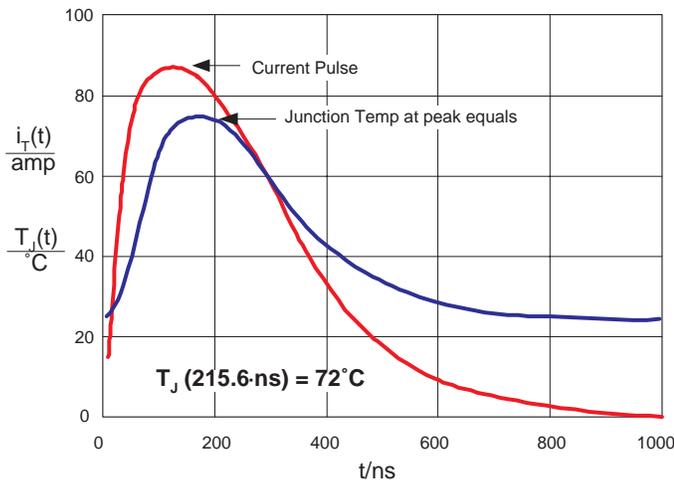
The current pulse  $i_T(t)$ , the SCR forward voltage  $P_T(t)$  and the junction temperature  $T_J(t)$  are shown in the accompanying graphs. The calculations may be performed on a spread sheet, using the piece-wise approach described above.

Fusing of the internal wires is not an issue for narrow current pulses for the wire size used in the device. The DC fuse rating is 18A and at a pulse width of 150ns, the fusing current limit is 2,483A.



Example 1

Half-Sine non-repetitive current pulse applied to a low resistance load in series with the anode of the UPGA301A. The graph illustrates the half-sine current pulse commencing from the point just after the combined delay and rise time of the SCR. The lower trace in the graph shows the junction temperature response. The peak junction temperature occurs at 148ns.



Example 2

A current pulse generated from a capacitor discharge through the UPGA301A with a low impedance load in series. Note the SCR presents a non-linear impedance to the current pulse. The graph shows the current pulse with a peak of 85.5A at 125ns. The lower trace shows the junction temperature response with a peak of 72°C at 216ns.