# RTAXS Single Event Effects Test Report 

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## SUMMARY

Prototype RTAXS devices were beam-tested at BNL and TAMU for single event effects (SEE), which include single event upset (SEU), single event functional interrupt (SEFI), single event latch-up (SEL) and single event dielectric rupture (SEDR). The key results are list below:

- The SEU-hardened TMR flip-flop (R-cell) meets the hardening target. The SEU rate per flip-flop at geostationary orbit for 100 mil aluminum shielding and solar-minimum environment is below $1.96 \times 10^{-11}$ upsets/bit•day.
- There is no occurrence of SEFI in any test run.
- There is no occurrence of SEL in any test run. The maximum effective LET used at BNL is $104 \mathrm{MeV} \cdot \mathrm{cm}^{2} / \mathrm{mg}$, and the maximum effective LET used at TAMU is $84 \mathrm{MeV} \cdot \mathrm{cm}^{2} / \mathrm{mg}$.
- There is no occurrence of SEDR in any test run. The maximum LET used at BNL is $60 \mathrm{MeV} \cdot \mathrm{cm}^{2} / \mathrm{mg}$, and the maximum LET used at TAMU is $54 \mathrm{MeV} \cdot \mathrm{cm}^{2} / \mathrm{mg}$.


## I. Test ObJective

This report combines the results of three heavy-ion-beam tests. The primary objective of these tests is to quantitatively characterize the SEE (single event effects) of the RTAXS product family. The SEE includes SEU (single event upset), SEFI (single event functional interrupt), SEL (single event latch-up) and SEDR (single event dielectric rupture). Particularly, the SEU cross-sections of the storage devices have to be obtained by the beam test. There are two storage devices in RTAXS product: the embedded RAM is reported in another separate report; the testing and analysis of the SEU-hardened TMR flip-flop in the logic module are described in this report.

## II. DEVICE UndER TEST

The devices under test (DUT) are separated into three groups by three separate heavy-ion-beam tests: Group A is made of samples from the first prototype (revision A) device, and this group is tested at BNL; Group B is made of samples from the revised prototype (revision B) device, also tested at BNL; Group C is also made of samples from the revision B prototype, and this group is tested at TAMU. For SEE point of view, revision A and revision B prototypes are practically the same, and they are treated as the same in this report. Table I lists the DUT parameters for each testing group.

Table I. DUT Parameters

|  | Group A | Group B | Group C |
| :---: | :---: | :---: | :---: |
| Device | RTAX2000S | RTAX2000S | RTAX1000S |
| Package | CQFP352 | CQFP352 | CQFP352 |
| Foundry | UMC | UMC | UMC |
| Technology | $0.15 \mu \mathrm{~m}$ CMOS | $0.15 \mu \mathrm{~m} \mathrm{CMOS}$ | $0.15 \mu \mathrm{~m} \mathrm{CMOS}$ |
| Die Size | $18.3 \mathrm{~mm} \times 16.9 \mathrm{~mm}$ | $18.3 \mathrm{~mm} \times 16.9 \mathrm{~mm}$ | $14.4 \mathrm{~mm} \times 13.3 \mathrm{~mm}$ |
| Die Lot Number | Rev A prototype | Rev B prototype | Rev B prototype |
| Date Code | NA | NA | NA |
| Quantity Tested | 2 | 4 | 3 |
| Serial Number | 307,315 | $\# 1, \# 2, \# 3, \# 4$ | $35475,35546,35551$ |
| IO Configuration | $3.3 V$ PCI | 3.3 V PCI | 3.3 V PCI |
| Design | TMRAXS | TMRAXS | TMRAXS |

## III. Test Methods

This test generally follows the guidelines of two SEE testing standards: ASTM standard F1192M-95, "Standard Guide for the Measurement of Single Event Phenomena (SEP) Induced by Heavy Ion Irradiation on Semiconductor Devices," and JEDEC standard JESD57, "Test Procedures for the Measurement of Single-Event Effects in Semiconductor Devices from Heavy Ion Irradiation."

Specifically, the SEU cross-section is obtained by measuring the in-flux upsets in two shift registers; the SEFI is monitored by the functionality of the shift registers; the SEL and SEDR are tested by measuring the in-flux power supply currents.

## A. Irradiation

Group-A and Group-B testing use the Tandem Van de Graaff beam source at Brookhaven National Laboratory; Group-C testing uses the Cyclotron beam source at Texas A\&M University. The irradiation details for each run are listed in Table II, III, and IV.

## B. Test Logic Design

The test logic design, called TMRAXS, composes of two shift registers, SH1 and SH2; each shift register has 100 stages (flip-flops), and each stage is made of one R-cell. Thus the upsets in these registers can be directly translated into the upsets in R-cells, and the SEU cross-section of the R-cell for a specific LET can be calculated.

## C. Experimental Setup and Procedure

Figure 1 shows the block diagram of the testing system. A PC (personal computer) commands the communication between an IO-counter card, which is plugged in a PCI slot on the motherboard, and a DUT board. The IO initiates the operation by starting the generator in the control chip to generate the clock and signal patterns. The signals passing the DUT and a control path are checked in the comparator; the generated errors are fed back into a counter on the IO-counter card. A heavy-ion beam of 1" diameter irradiates only the DUT chip on the DUT board. The communication between the IO-counter and DUT board is through RS422 interfaces.

The data generator generates " 1 ", " 0 ", or checkerboard patterns. The checkerboard pattern is used for detecting SEU because it toggles every flip-flop at the clock edge and it also can detect the "clock" upset. An HP6629 power supply unit is used to monitor the in-flux current for SEL and SEDR detection. This power supply communicates with the PC through a GPIB interface so that the in-flux power supply current is recorded throughout the testing. For the worst case scenario, the power supply voltage is $10 \%$ under nominal for SEU testing and $10 \%$ over nominal for SEL and SEDR testing.


Figure 1 Block diagram showing the measurement of upset-errors

## IV. RESULTS AND DISCUSSIONS

A. Test Data

Tables II, III and IV list the Group-A, Group-B and Group-C test data respectively. Key results are:

1. Upsets for each run to the fluence of $10^{7} \mathrm{Ions} / \mathrm{cm}^{2}$ are low, even for high LETs.
2. The upsets at $0^{\circ}$ roll and $90^{\circ}$ roll is approximately the same. As shown in Figure 2, the TMR flip-flop has three sub-flip-flops stacked vertically. Rolling $90^{\circ}$ and tilting will enhance the possibility of the TMR flipflop upset by ion striking two sub-flip-flops the same time. The distance between the sub-flip-flops is designed to avoid this upset mechanism, which is consistent with the testing result.


Figure 2 Simplified drawings showing the relative position of the sub-flip-flops in the TMR flip-flop with respect to the roll and tilt angles.
3. Several runs in Group C show the multiple upsets symptom, indicating the possibility of clock upset; particularly run 12 in Group C shows a burst of 28 errors in SH2. However, this error-burst case could not be reproduced by repeating test runs. Since these suspected multiple-upsets are occurred at a very high LET of $62.8 \mathrm{MeV} \cdot \mathrm{cm}^{2} / \mathrm{mg}$, the impact to the upset rate in the standard GEO environment is negligible.
4. There is no occurrence of SEFI in any run.
5. There is no occurrence of SEL in any run.
6. There is no occurrence of SEDR in any run.

Table II. Group-A Test Data

| BNL | DUT | Bias (V) | Ion | LET | Tilt | Flux | Fluence |  |  | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Run | DUT | $\mathrm{V}_{\mathrm{CCI}} / \mathrm{V}_{\mathrm{CCA}}$ | Ion | $\left(\mathrm{MeV} \cdot \mathrm{~cm}^{2} / \mathrm{mg}\right)$ | Tilt | $\text { (Ions } / \mathrm{cm}^{2} / \mathrm{s} \text { ) }$ | (Ions/cm ${ }^{2}$ ) | SR1 | SR2 |  |
| 298 | 307 | 3.3/1.5 | Br-81 | 37.45 | 0 | $2.37 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 1 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 299 | 307 | 3.3/1.5 | Br-81 | 52.96 | 45 | $2.44 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 1 | 1 | CB, 2 MHz |
| 300 | 307 | 3.3/1.5 | Br-81 | 52.96 | -45 | $2.67 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 1 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 301 | 307 | 3.3/1.5 | I-127 | 59.73 | 0 | $1.78 \mathrm{E}+04$ | $8.86 \mathrm{E}+06$ | 1 | 0 | CB, 2 MHz |
| 302 | 307 | 3.3/1.5 | I-127 | 68.98 | 30 | $1.59 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 303 | 307 | 3.3/1.5 | I-127 | 84.48 | 45 | $1.11 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 1 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 304 | 307 | 3.3/1.5 | I-127 | 104.1 | 55 | $8.99 \mathrm{E}+03$ | $1.00 \mathrm{E}+07$ | 0 | 1 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 305 | 307 | 3.3/1.5 | I-127 | 68.98 | -30 | $1.28 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 306 | 307 | 3.3/1.5 | I-127 | 84.48 | -45 | $3.17 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 1 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 307 | 307 | 3.3/1.5 | I-127 | 92.93 | -50 | $2.68 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB, 2 MHz |
| 308 | 315 | 3.3/1.5 | I-127 | 59.73 | 0 | $4.38 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 1 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 309 | 315 | 3.3/1.5 | I-127 | 68.98 | 30 | $3.70 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 310 | 315 | 3.3/1.5 | I-127 | 84.48 | 45 | $2.53 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 2 | 0 | CB, 2 MHz |
| 311 | 315 | 3.3/1.5 | I-127 | 104.1 | 55 | $2.25 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB, 2 MHz |
| 312 | 315 | 3.3/1.5 | I-127 | 68.98 | -30 | $3.25 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 2 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 313 | 315 | 3.3/1.5 | I-127 | 84.48 | -45 | $2.28 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB, 2 MHz |
| 314 | 315 | 3.3/1.5 | Ni-58 | 26.58 | 0 | $4.14 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 1 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 315 | 315 | 3.3/1.5 | Ni-58 | 30.69 | 30 | $4.76 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 316 | 315 | 3.3/1.5 | Ni-58 | 37.59 | 45 | $3.66 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 317 | 315 | 3.3/1.5 | Ni-58 | 30.7 | -30 | $5.05 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 1 | CB, 2 MHz |
| 318 | 315 | 3.3/1.5 | Ni-58 | 37.59 | -45 | $4.34 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 319 | 307 | 3.3/1.5 | Ni-58 | 26.58 | 0 | $3.56 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB, 2 MHz |
| 320 | 307 | 3.3/1.5 | Ni-58 | 30.69 | 30 | $4.00 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 321 | 307 | 3.3/1.5 | Ni-58 | 37.59 | 45 | $3.40 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 1 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 322 | 307 | 3.3/1.5 | Ni-58 | 30.69 | -30 | $4.29 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 1 | 1 | CB, 2 MHz |
| 323 | 307 | 3.3/1.5 | Ni-58 | 37.59 | -45 | $3.49 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |

Table III. Group-B Test Data

| BNL Run | DUT | Bias (V) | Ion | LET | Tilt | Roll | Flux | $\begin{gathered} \text { Fluence } \\ \text { (Ions/ } / \mathrm{cm}^{2} \text { ) } \end{gathered}$ | Upsets |  | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\mathrm{V}_{\mathrm{CCI}} / \mathrm{V}_{\mathrm{CCA}}$ |  | $\left(\mathrm{MeV} \cdot \mathrm{cm}^{2} / \mathrm{mg}\right)$ | (Deg) | (Deg) | (Ions/ $\mathrm{cm}^{2} / \mathrm{s}$ ) |  | SH1 | SH2 |  |
| 100 | \#1 | 3.3/1.5 | Br-81 | 37.46 | 0 | 0 | $1.97 \mathrm{E}+05$ | $1.01 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 101 | \#1 | 3.3/1.5 | Br-81 | 37.46 | 0 | 0 | $1.12 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 1 | CB, 2 MHz |
| 102 | \#1 | 3.0/1.4 | Br-81 | 37.46 | 0 | 0 | $1.19 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 103 | \#1 | 3.0/1.4 | Br-81 | 52.98 | 45 | 0 | $8.41 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 1 | 0 | CB, 2MHz |
| 104 | \#1 | 3.0/1.4 | Br-81 | 52.97 | 45 | 0 | $8.11 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 1 | 0 | CB, 2 MHz |
| 105 | \#2 | 3.0/1.4 | Br-81 | 37.46 | 0 | 0 | $6.28 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 1 | 0 | CB, 2 MHz |
| 106 | \#2 | 3.0/1.4 | Br-81 | 52.98 | 45 | 0 | $3.18 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 107 | \#2 | 3.0/1.4 | Br-81 | 52.98 | -45 | 0 | $2.49 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 1 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 108 | \#2 | 3.0/1.4 | Br-81 | 37.46 | 0 | -89.1 | $2.71 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 109 | \#2 | 3.0/1.4 | Br-81 | 52.98 | 45 | -89.1 | $2.43 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 1 | 0 | CB, 2 MHz |
| 110 | \#2 | 3.0/1.4 | Br-81 | 52.98 | -45 | -89.1 | $1.81 \mathrm{E}+04$ | $6.52 \mathrm{E}+05$ | NA | NA | Aborted |
| 111 | \#2 | 3.0/1.4 | Br-81 | 52.98 | -45 | -89.1 | $2.31 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB, 2 MHz |
| 112 | \#2 | 3.0/1.4 | Br-81 | 43.25 | -30 | -89.1 | $9.71 \mathrm{E}+04$ | $1.01 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 113 | \#2 | 3.0/1.4 | Br-81 | 43.25 | -30 | -89.1 | $9.59 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 1 | CB, 2 MHz |
| 114 | \#2 | 3.0/1.4 | Br-81 | 43.25 | 30 | -89.1 | $9.54 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB, 2MHz |
| 115 | \#3 | 3.0/1.4 | Br-81 | 37.46 | 0 | 0 | $1.10 \mathrm{E}+05$ | $1.01 \mathrm{E}+07$ | 1 | 1 | CB, 2 MHz |
| 116 | \#3 | 3.0/1.4 | Br-81 | 37.46 | 0 | 0 | $1.13 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 117 | \#3 | 3.0/1.4 | Br-81 | 43.25 | 30 | 0 | $9.64 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 1 | 1 | CB, 2 MHz |
| 118 | \#3 | 3.0/1.4 | Br-81 | 43.25 | 30 | 0 | $9.60 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 2 | 1 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 119 | \#3 | 3.0/1.4 | Br-81 | 43.25 | 30 | 0 | $4.32 \mathrm{E}+04$ | $9.98 \mathrm{E}+06$ | 2 | 1 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 120 | \#3 | 3.0/1.4 | Br-81 | 43.25 | -30 | 0 | $4.01 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 1 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 121 | \#3 | 3.0/1.4 | Br-81 | 52.98 | 45 | 0 | $2.90 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB, 2MHz |
| 122 | \#3 | 3.0/1.4 | Br-81 | 52.98 | 45 | 0 | $2.85 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 1 | 0 | CB, 2MHz |
| 123 | \#3 | 3.0/1.4 | Br-81 | 52.98 | -45 | 0 | $3.10 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 1 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 124 | \#3 | 3.0/1.4 | Br-81 | 43.25 | 30 | -89 | $3.95 \mathrm{E}+04$ | $9.95 \mathrm{E}+06$ | 1 | 0 | CB, 2 MHz |
| 125 | \#3 | 3.0/1.4 | Br-81 | 43.25 | -30 | -89 | $4.11 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 2 | 0 | CB, 2MHz |
| 126 | \#3 | 3.0/1.4 | Br-81 | 52.98 | -45 | -89 | $3.22 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 127 | \#3 | 3.0/1.4 | Br-81 | 52.98 | 45 | -89 | $3.19 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB, 2MHz |
| 128 | \#3 | 3.0/1.4 | Br-81 | 52.98 | 45 | -89 | $3.01 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 1 | One, 2 MHz |
| 129 | \#4 | 3.0/1.4 | Br-81 | 37.46 | 0 | 0 | $6.27 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 1 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 130 | \#4 | 3.0/1.4 | Br-81 | 43.25 | 30 | 0 | $8.65 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 131 | \#4 | 3.0/1.4 | Br-81 | 52.98 | 45 | 0 | $7.06 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 3 | 0 | CB, 2MHz |
| 132 | \#4 | 3.0/1.4 | Br-81 | 43.25 | -30 | 0 | $8.38 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 133 | \#4 | 3.0/1.4 | Br-81 | 52.97 | -45 | 0 | $6.82 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 1 | 1 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 134 | \#4 | 3.0/1.4 | I-127 | 59.72 | 0 | 0 | $5.58 \mathrm{E}+04$ | $9.54 \mathrm{E}+06$ | 2 | 1 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 135 | \#4 | 3.0/1.4 | I-127 | 68.96 | 30 | 0 | $4.57 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 1 | 0 | CB, 2 MHz |
| 136 | \#4 | 3.0/1.4 | I-127 | 84.46 | 45 | 0 | $3.49 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 3 | CB, 2MHz |
| 137 | \#4 | 3.0/1.4 | I-127 | 68.96 | -30 | 0 | $3.89 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 1 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 138 | \#4 | 3.0/1.4 | I-127 | 84.45 | -45 | 0 | $2.97 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 1 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 139 | \#4 | 3.6/1.65 | I-127 | 84.45 | -45 | 0 | $2.79 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | No SEL, No SEDR |
| 140 | \#4 | 3.6/1.65 | I-127 | 84.46 | 45 | 0 | $7.08 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | No SEL, No SEDR |
| 141 | \#4 | 3.6/1.65 | I-127 | 104.1 | 55 | 0 | $4.80 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | No SEL, No SEDR |
| 142 | \#4 | 3.6/1.65 | I-127 | 104.1 | -55 | 0 | $4.75 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | No SEL, No SEDR |
| 143 | \#4 | 3.6/1.65 | I-127 | 59.72 | 0 | 0 | $7.74 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 1 | 0 | No SEL, No SEDR |
| 144 | \#3 | 3.0/1.4 | I-127 | 59.72 | 0 | 0 | $6.91 \mathrm{E}+04$ | $9.98 \mathrm{E}+06$ | 2 | 1 | CB, 2MHz |
| 145 | \#3 | 3.0/1.4 | I-127 | 68.96 | 30 | 0 | $5.39 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 146 | \#3 | 3.0/1.4 | I-127 | 84.46 | 45 | 0 | $4.12 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB, 2MHz |
| 147 | \#3 | 3.6/1.65 | I-127 | 104.1 | 55 | 0 | $3.30 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | No SEL, No SEDR |
| 148 | \#3 | 3.6/1.65 | I-127 | 104.1 | -55 | 0 | $3.08 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | No SEL, No SEDR |
| 149 | \#3 | 3.6/1.65 | I-127 | 104.1 | -55 | 0 | $2.81 \mathrm{E}+04$ | $9.95 \mathrm{E}+06$ | 0 | 0 | No SEL, No SEDR |
| 150 | \#3 | 3.6/1.65 | I-127 | 59.72 | 0 | 0 | $4.66 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 2 | 0 | No SEL, No SEDR |
| 151 | \#2 | 3.0/1.4 | I-127 | 59.72 | 0 | 0 | $9.33 \mathrm{E}+04$ | $1.01 \mathrm{E}+07$ | 2 | 0 | CB, 2 MHz |
| 152 | \#2 | 3.0/1.4 | I-127 | 68.96 | 30 | 0 | $7.55 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 1 | 0 | CB, 2MHz |
| 153 | \#2 | 3.0/1.4 | I-127 | 84.46 | 45 | 0 | $5.81 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB, 2 MHz |
| 154 | \#2 | 3.6/1.65 | I-127 | 104.1 | 55 | 0 | $4.07 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | No SEL, No SEDR |
| 155 | \#2 | 3.6/1.65 | I-127 | 104.1 | -55 | 0 | $3.62 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | No SEL, No SEDR |


| 156 | \#2 | 3.6/1.65 | I-127 | 59.72 | 0 | 0 | $5.37 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | No SEL, No SEDR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 157 | \#1 | 3.0/1.4 | I-127 | 59.72 | 0 | 0 | $1.19 \mathrm{E}+05$ | $9.95 \mathrm{E}+06$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 158 | \#1 | 3.0/1.4 | I-127 | 68.96 | 30 | 0 | $1.01 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 159 | \#1 | 3.0/1.4 | I-127 | 84.45 | 45 | 0 | $1.01 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 160 | \#1 | 3.6/1.65 | I-127 | 104.1 | 55 | 0 | $2.48 \mathrm{E}+04$ | $1.01 \mathrm{E}+07$ | 0 | 0 | No SEL, No SEDR |
| 161 | \#1 | 3.6/1.65 | I-127 | 104.1 | -55 | 0 | $4.25 \mathrm{E}+04$ | $9.89 \mathrm{E}+06$ | 0 | 0 | No SEL, No SEDR |
| 162 | \#1 | 3.6/1.65 | I-127 | 59.72 | 0 | 0 | $4.63 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 2 | 0 | No SEL, No SEDR |
| 163 | \#1 | 3.0/1.4 | Cl-35 | 11.73 | 0 | 0 | $1.45 \mathrm{E}+05$ | $1.01 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 164 | \#1 | 3.0/1.4 | Cl-35 | 13.54 | 30 | 0 | $1.26 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 165 | \#1 | 3.0/1.4 | Cl-35 | 16.59 | 45 | 0 | $1.02 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 166 | \#1 | 3.0/1.4 | Cl-35 | 13.54 | -30 | 0 | $1.26 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB, 2 MHz |
| 167 | \#1 | 3.0/1.4 | Cl-35 | 16.59 | -45 | 0 | $1.02 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB, 2 MHz |
| 168 | \#1 | 3.0/1.4 | Cl-35 | 13.54 | 30 | -89 | $1.25 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 169 | \#1 | 3.0/1.4 | Cl-35 | 16.59 | 45 | -89 | $1.01 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 170 | \#2 | 3.0/1.4 | Cl-35 | 11.73 | 0 | 0 | $1.43 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 171 | \#2 | 3.0/1.4 | Cl-35 | 13.54 | 30 | 0 | $1.24 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 172 | \#2 | 3.0/1.4 | Cl-35 | 16.59 | 45 | 0 | $1.01 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 1 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 173 | \#2 | 3.0/1.4 | Cl-35 | 16.59 | -45 | 0 | $9.96 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB, 2 MHz |
| 174 | \#2 | 3.0/1.4 | Cl-35 | 13.54 | -30 | 0 | $1.22 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 1 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 175 | \#2 | 3.0/1.4 | Cl-35 | 13.54 | 30 | -89 | $1.23 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 176 | \#2 | 3.0/1.4 | Cl-35 | 16.59 | 45 | -89 | $1.01 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 177 | \#2 | 3.0/1.4 | Cl-35 | 16.59 | -45 | -89 | $1.01 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 178 | \#2 | 3.0/1.4 | Cl-35 | 13.54 | -30 | -89 | $1.25 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB, 2 MHz |
| 179 | \#3 | 3.0/1.4 | Cl-35 | 11.73 | 0 | 0 | $1.45 \mathrm{E}+05$ | $1.01 \mathrm{E}+07$ | 0 | 0 | CB, 2 MHz |
| 180 | \#3 | 3.0/1.4 | Cl-35 | 16.59 | 45 | 0 | $1.03 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB, 2MHz |
| 181 | \#3 | 3.0/1.4 | Cl-35 | 13.54 | 30 | 0 | $1.26 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 183 | \#4 | 3.0/1.4 | Cl-35 | 16.59 | 45 | 0 | $1.03 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 184 | \#4 | 3.0/1.4 | Cl-35 | 13.54 | 30 | 0 | $1.28 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB, 2MHz |
| 185 | \#4 | 3.0/1.4 | Cl-35 | 11.73 | 0 | 0 | $1.47 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 186 | \#4 | 3.0/1.4 | Ni-58 | 26.58 | 0 | 0 | $1.14 \mathrm{E}+05$ | $1.06 \mathrm{E}+07$ | 0 | 0 | CB, 2 MHz |
| 187 | \#4 | 3.0/1.4 | Ni -58 | 30.69 | 30 | 0 | $1.03 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 188 | \#4 | 3.0/1.4 | Ni-58 | 37.59 | 45 | 0 | $8.49 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 189 | \#4 | 3.0/1.4 | Ni-58 | 37.59 | -45 | 0 | $8.83 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 1 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 190 | \#4 | 3.0/1.4 | Ni-58 | 30.69 | -30 | 0 | $1.05 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 1 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 191 | \#3 | 3.0/1.4 | Ni-58 | 26.58 | 0 | 0 | $1.32 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 1 | 0 | CB, 2 MHz |
| 192 | \#3 | 3.0/1.4 | Ni-58 | 30.69 | 30 | 0 | $1.10 \mathrm{E}+05$ | $9.99 \mathrm{E}+06$ | 0 | 0 | CB, 2 MHz |
| 193 | \#3 | 3.0/1.4 | Ni-58 | 30.69 | -30 | 0 | $1.07 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 1 | 1 | CB, 2 MHz |
| 194 | \#2 | 3.0/1.4 | Ni-58 | 30.69 | -30 | 0 | $1.11 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB, 2 MHz |
| 195 | \#2 | 3.0/1.4 | Ni-58 | 26.58 | 0 | 0 | $1.25 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB, 2MHz |
| 196 | \#2 | 3.0/1.4 | Ni-58 | 30.69 | 30 | 0 | $1.05 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 1 | CB, 2MHz |
| 197 | \#2 | 3.0/1.4 | Ni-58 | 30.69 | 30 | 0 | $1.05 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 198 | \#1 | 3.0/1.4 | Ni-58 | 30.69 | -30 | 0 | $6.16 \mathrm{E}+04$ | $1.01 \mathrm{E}+07$ | 0 | 0 | CB, 2 MHz |
| 199 | \#1 | 3.0/1.4 | Ni-58 | 26.58 | 0 | 0 | $7.24 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 1 | $\mathrm{CB}, 2 \mathrm{MHz}$ |
| 200 | \#1 | 3.0/1.4 | Ni-58 | 30.69 | 30 | 0 | $4.31 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 1 | CB, 2 MHz |
| 201 | \#1 | 3.0/1.4 | Ni-58 | 30.69 | 30 | 0 | $3.89 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB, 2 MHz |
| 202 | \#1 | 3.0/1.4 | Ni-58 | 26.58 | 0 | 0 | $3.60 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | $\mathrm{CB}, 2 \mathrm{MHz}$ |

Table IV. Group-C Test Data

| $\begin{aligned} & \text { TAMU } \\ & \text { Run } \end{aligned}$ | DUT | Bias (V) | Ion | $\overline{\text { LET }}$ | Tilt | Flux | Fluence (Ions/cm ${ }^{2}$ ) | Upset |  | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | $\mathrm{V}_{\mathrm{CCI}} / \mathrm{V}_{\text {CCA }}$ |  | $\left(\mathrm{MeV} \cdot \mathrm{~cm}^{2} / \mathrm{mg}\right)$ |  | $\text { (Ions } / \mathrm{cm}^{2} / \mathrm{s} \text { ) }$ |  | SH1 | SH2 |  |
| 1 | 35546 | 3.3/1.5 | Ag | 44.4 | 0 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 1 | 0 | zero pattern 2 MHz |
| 2 | 35546 | 3.3/1.35 | Ag | 44.4 | 0 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 1 | 0 | CB 2MHz |
| 3 | 35546 | 3.0/1.35 | Ag | 44.4 | 0 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB 2MHz |
| 4 | 35546 | 3.6/1.7 | Ag | 44.4 | 0 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB 2MHz |
| 5 | 35546 | 3.6/1.7 | Ag | 62.8 | 45 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 2 | 2 | CB 2MHz |
| 6 | 35546 | 3.6/1.7 | Ag | 69 | 50 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB 2MHz |
| 7 | 35546 | 3.0/1.35 | Ag | 69 | 50 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 1 | 1 | CB 2MHz |
| 8 | 35546 | 3.0/1.35 | Ag | 62.8 | 45 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB 2MHz |
| 9 | 35546 | 3.0/1.35 | Ag | 51.3 | 30 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 1 | 0 | CB 2MHz |
| 10 | 35546 | 3.0/1.35 | Ag | 51.3 | 30 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB 500 kHz |
| 11 | 35546 | 3.0/1.35 | Ag | 51.3 | 30 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB 100 kHz |
| 12 | 35546 | 3.0/1.35 | Ag | 62.8 | 45 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 1 | 28 | CB 100 kHz , clock upset? |
| 13 | 35546 | 3.0/1.35 | Ag | 62.8 | 45 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 1 | 1 | CB 100 kHz , clock upset? |
| 14 | 35475 | 3.0/1.35 | Ag | 44.4 | 0 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | Zero 2MHz |
| 15 | 35475 | 3.0/1.35 | Ag | 44.4 | 0 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB 2MHz |
| 16 | 35475 | 3.6/1.7 | Ag | 44.4 | 0 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 2 | CB 2MHz |
| 17 | 35475 | 3.6/1.7 | Ag | 62.8 | 45 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB 2MHz |
| 18 | 35475 | 3.0/1.35 | Ag | 62.8 | 45 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB 2MHz |
| 19 | 35475 | 3.0/1.35 | Ag | 62.8 | 45 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB 100 kHz |
| 20 | 35475 | 3.0/1.35 | Ag | 51.3 | 30 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB 100 kHz |
| 21 | 35475 | 3.0/1.35 | Ag | 44.4 | 0 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB 100kHz |
| 22 | 35551 | 3.0/1.35 | Ag | 44.4 | 0 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | Zero 100 kHz |
| 23 | 35551 | 3.0/1.35 | Ag | 44.4 | 0 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB 100 kHz |
| 24 | 35551 | 3.6/1.7 | Ag | 44.4 | 0 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB 100 kHz |
| 25 | 35551 | 3.6/1.7 | Ag | 62.8 | 45 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB 100 kHz |
| 26 | 35551 | 3.6/1.7 | Ag | 62.8 | 45 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB 100kHz |
| 27 | 35551 | 3.0/1.35 | Ag | 62.8 | 45 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB 100kHz |
| 28 | 35551 | 3.0/1.35 | Ag | 62.8 | 45 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 1 | 1 | CB 2MHz, clock upset? |
| 29 | 35551 | 3.6/1.7 | Ag | 62.8 | 45 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB 2 MHz |
| 30 | 35551 | 3.6/1.7 | Ag | 44.4 | 0 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 1 | 0 | CB 2MHz |
| 31 | 35551 | 3.0/1.35 | Ag | 44.4 | 0 | $1.00 \mathrm{E}+05$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB 2MHz |
| 63 | 35475 | 3.0/1.35 | Xe | 54 | 0 | $6.00 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 1 | 1 | CB 2MHz |
| 64 | 35475 | 3.0/1.35 | Xe | 54 | 0 | $6.00 \mathrm{E}+04$ | $6.00 \mathrm{E}+06$ | 0 | 0 | CB 2MHz |
| 65 | 35475 | 3.6/1.7 | Xe | 54 | 0 | $6.00 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB 2 MHz |
| 66 | 35475 | 3.6/1.7 | Xe | 76.4 | 45 | $6.00 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB 2MHz |
| 67 | 35475 | 3.0/1.35 | Xe | 76.4 | 45 | $6.00 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 1 | CB 2MHz |
| 68 | 35475 | 3.0/1.35 | Xe | 84 | 50 | $6.00 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 1 | CB 2MHz |
| 69 | 35475 | 3.6/1.7 | Xe | 84 | 50 | $6.00 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 1 | CB 2MHz |
| 70 | 35546 | 3.6/1.7 | Xe | 54 | 0 | $6.00 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 2 | 0 | CB 2MHz |
| 71 | 35546 | 3.0/1.35 | Xe | 54 | 0 | $5.00 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 1 | CB 2MHz |
| 72 | 35546 | 3.0/1.35 | Xe | 84 | 50 | $5.00 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB 2MHz |
| 73 | 35546 | 3.6/1.7 | Xe | 84 | 50 | $5.00 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 1 | CB 2MHz |
| 74 | 35551 | 3.6/1.7 | Xe | 54 | 0 | $5.00 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 0 | CB 2MHz |
| 75 | 35551 | 3.6/1.7 | Xe | 84 | 50 | $5.00 \mathrm{E}+04$ | $1.00 \mathrm{E}+07$ | 0 | 1 | CB 2MHz |

## B. Single Event Upset and Rate Prediction

Group-B test data acquired are used to obtain the SEU cross-section because this group has the most complete data. Figure 2 shows the cross-section per flip-flop calculated from the upsets measured for each specific LET. Each data point is the average upset of the four DUTs. The measured errors may include facility noises (e.g. mechanical noises). Nevertheless, all the measured errors are counted for a worst-case scenario. The Weibull-curve fit of these data obtains: $\mathrm{L}_{0}=10 \mathrm{MeV} \cdot \mathrm{cm} 2 / \mathrm{mg}$; width $=35 \mathrm{MeV} \cdot \mathrm{cm} 2 / \mathrm{mg}$; shape $=2$; saturation crosssection $=9 \times 10^{-10} \mathrm{~cm}^{2}$. The approximate device parameters for simulation are: active volume depth $=0.15 \mu \mathrm{~m}$, and funnel depth $=0.3 \mu \mathrm{~m}$. Using Space Radiation 4.5 simulator with Weibull and device parameters, the SEU rate at GEO for 100 mil Aluminum shielding and Solar minimum condition is obtained as $1.96 \times 10^{-11}$ upsets/bit•day.

Group-A and Group-C test data are consistent with the above data. Group-C test data also includes upsets measured both at $100-\mathrm{kHz}$ and $2-\mathrm{MHz}$ clock speed. Except the outlier of Run 12, the $100-\mathrm{kHz}$ upsets are significantly less than the $2-\mathrm{MHz}$ upsets; this indicates that the measured upsets are mostly single-event-transient induced.


Figure 3 Group-B test data plotted as the SEU Cross-section of the TMR flip-flop with respect to the heavyion LET, each data point represents the average of four DUTs. The data point with an arrow pointed down-ward indicates the cross-section derived from test data is below this point. The curve is a Weibull fit for SEU rate predictions.


Figure 4 Group-A test data plotted as the SEU cross-section of the TMR flip-flop with respect to the heavy ion LET.


Figure 5 Group-C test data plotted as the SEU cross-section of the TMR flip-flop with respect to the heavy ion LET.

## C. Single Event Latch-up

There is no occurrence of SEL in any Group-A, Group-B or Group-C test run. Table V lists the SEL testing limits for each test Group.

Table V SEL Testing Limits

|  | Group A | Group B | Group C |
| :--- | :--- | :--- | :--- |
| Facility | BNL | BNL | TAMU |
| $\mathrm{V}_{\mathrm{CCI}} / \mathrm{V}_{\mathrm{CCA}}$ | $3.3 \mathrm{~V} / 1.5 \mathrm{~V}$ | $3.6 \mathrm{~V} / 1.65 \mathrm{~V}$ | $3.6 \mathrm{~V} / 1.7 \mathrm{~V}$ |
| Temperature | Room | Room | Room |
| Max Effective LET <br> $\left(\mathrm{MeV} \cdot \mathrm{cm}^{2} / \mathrm{mg}\right)$ | $104(320-\mathrm{MeV}$ <br> Iodine tilted $\left.55^{\circ}\right)$ | $104(320-\mathrm{MeV}$ <br> Iodine tilted $\left.55^{\circ}\right)$ | $84(1.253-\mathrm{GeV} \mathrm{Xe}$ <br> tilted $\left.50^{\circ}\right)$ |
| Quantity Tested | 2 | 4 | 3 |

## D. Single Event Dielectric Rupture

The signature of the occurrence of a SEDR is a permanent power-supply current jump. Based on previous experiences the resistance of the antifuse after SEDR is approximately $500-1000 \Omega$, so the current jump is 1.5 V $\left(\mathrm{V}_{\mathrm{CCA}}\right) / 500-1000 \Omega$, which is $3 \mathrm{~mA}-1.5 \mathrm{~mA}$. Since the antifuse can only be biased by $\mathrm{V}_{\text {CCA }}$, the in-flux $\mathrm{I}_{\mathrm{CCA}}$ is examined throughout the test run. Figures $5-8$ show the in-flux $I_{\text {CCA }}$ for the Group-B SEDR testing runs, and Figures $9-11$ show the in-flux $\mathrm{I}_{\mathrm{CCA}}$ for the Group-C SEDR testing runs. No signature permanent current jump is observed in any run. The maximum LET for Group-B testing is $60 \mathrm{MeV} \cdot \mathrm{cm}^{2} / \mathrm{mg}$ (Iodine), and for Group-C testing is $54 \mathrm{MeV} \cdot \mathrm{cm}^{2} / \mathrm{mg}(\mathrm{Xe})$. The worst case for SEDR is with the ion beam perpendicular to the antifuse surface; an ion with small LET striking at a tilting angle cannot be used to simulate the effect of an ion-strike with a large LET. Since the antifuse surface is not completely perpendicular to the surface, tilting test runs with high LET ions are performed for completeness. The antifuse is between the top two layers of metal, so the penetration of heavy ions is not an issue.


Figure 6 Group-B DUT \#4 in-flux $\mathrm{I}_{\mathrm{CCA}}$ current, $\mathrm{V}_{\mathrm{CCA}}=1.65 \mathrm{~V}$. $\mathrm{I}_{\mathrm{CCA}}$ increases continuously because of total dose effect. $\mathrm{I}_{\mathrm{CCA}}$ also has small fluctuation but no significant jumps, which would be the signature of SEDR.


Figure 7 Group-B DUT \#3 in-flux $\mathrm{I}_{\mathrm{CCA}}$ current, $\mathrm{V}_{\mathrm{CCA}}=1.65 \mathrm{~V}$. $\mathrm{I}_{\mathrm{CCA}}$ increases continuously because of totaldose effect. $I_{\text {CCA }}$ also has small fluctuations but no significant permanent jumps, which would be the signature of SEDR.


Figure 8 Group-B DUT \#2 in-flux $\mathrm{I}_{\mathrm{CCA}}$ current, $\mathrm{V}_{\mathrm{CCA}}=1.65 \mathrm{~V}$. $\mathrm{I}_{\mathrm{CCA}}$ increases continuously because of totaldose effect. $\mathrm{I}_{\mathrm{CCA}}$ also has small fluctuations but no significant permanent jumps, which would be the signature of SEDR. Run- 156 has small temporary current-pulse of $\sim 0.5 \mathrm{~mA}$, which may due to charging/discharging effects.


Figure 9 Group-B DUT \#1 in-flux $\mathrm{I}_{\mathrm{CCA}}$ current, $\mathrm{V}_{\mathrm{CCA}}=1.65 \mathrm{~V}$. $\mathrm{I}_{\mathrm{CCA}}$ increases continuously because of totaldose effect. $\mathrm{I}_{\mathrm{CCA}}$ also has small fluctuations but no significant permanent jumps, which would be the signature of SEDR.


Figure 10 Group-C DUT 34475 in-flux $\mathrm{I}_{\mathrm{CCA}}$ current, $\mathrm{V}_{\mathrm{CCA}}=1.7 \mathrm{~V}$. $\mathrm{I}_{\mathrm{CCA}}$ increases continuously because of total-dose effect. $\mathrm{I}_{\mathrm{CCA}}$ also has small fluctuations but no significant permanent jumps, which would be the signature of SEDR.


Figure 11 Group-C DUT 35546 in-flux $\mathrm{I}_{\mathrm{CCA}}$ current, $\mathrm{V}_{\mathrm{CCA}}=1.7 \mathrm{~V}$. $\mathrm{I}_{\mathrm{CCA}}$ increases continuously because of total-dose effect. $\mathrm{I}_{\mathrm{CCA}}$ also has small fluctuations but no significant permanent jumps, which would be the signature of SEDR.


Figure 12 Group-C DUT 35551 in-flux $\mathrm{I}_{\mathrm{CCA}}$ current, $\mathrm{V}_{\mathrm{CCA}}=1.7 \mathrm{~V}$. $\mathrm{I}_{\mathrm{CCA}}$ increases continuously because of total-dose effect. $\mathrm{I}_{\mathrm{CCA}}$ also has small fluctuations but no significant permanent jumps, which would be the signature of SEDR.

