



RTAX-S TAMU Single Event Dielectric Rupture
August 8, 2006

J.J. Wang and S. Rezgui
(650) 318-4576
jih-jong.wang@actel.com

I. INTRODUCTION

Single event dielectric rupture (SEDR) was observed during a beam test on RTAX2000S devices. This phenomenon, although it has never been observed in any space-flight data, has been attributed to beam-induced antifuse rupture. The characteristics of the SEDR can be summarized as:

1. The SEDR event is identified by a small permanent jump in the core power supply current (I_{CCA}). Sometimes an I_{CCI} jump occurs simultaneously with an I_{CCA} jump. Since all the antifuses are biased by V_{CCA} only, the probable cause for this I_{CCI} jump is an induced current in the V_{CCI} -powered circuits due to an SEDR in the V_{CCA} -powered array.
2. The threshold LET is very high, in this case approximately $80 \text{ MeV}\cdot\text{cm}^2/\text{mg}$.
3. The DUT always continues to function after SEDR occurs.
4. In this case only one out of three DUT had SEDR occurring; and it occurred only at $V_{CC}+10\%$.
5. The worst-case incidence angle is 90° , or 0° -tilt.

In this document, the rate of SEDR is estimated for the worst-case space environment. Due to the rarity of the event, it is considered more of an academic curiosity than a practical risk.

II. DUT AND BEAM TEST

The details of the beam test can be found in a report, "RTAXS TAMU Single Event Latch-up Test Report" dated July 12, 2006. This report is available for download from the Actel web site at <http://www.actel.com/documents/RTAX-S%20High%20Temp%20SEL.pdf>. Table I lists the DUT parameters; Table II lists the test log; and Fig. 1 to Fig. 18 shows the in-flux I_{CC} of each run. SEDR events are identified in Fig. 7 and Fig. 9.

III. RATE CALCULATION

Integral flux hitting on a flat antifuse at all angles

$$\begin{aligned} &= \iint_{\text{sphere-surface}} F \cdot \cos \theta \cdot d\Omega \\ &= 2 \cdot \int_0^{2\pi} \int_0^{\frac{\pi}{2}} F \cdot \sin \theta \cdot \cos \theta \cdot d\theta d\phi \\ &= 2\pi \cdot F \text{ (ions}\cdot\text{m}^{-2}\cdot\text{s}^{-1}) \end{aligned}$$

F is the space integral flux ($\text{ions}\cdot\text{m}^{-2}\cdot\text{sr}^{-1}\cdot\text{s}^{-1}$) that can be simulated by CREME96. Fig. 19 shows the plot of F versus LET in a typical environment: geosynchronous orbit, solar minimum activity, and 100-mil Al shielding. Use the worst-case scenario of Fig. 7: four (4) SEDR occurred for total fluence of 10^7 cm^{-2} . The integral flux (F) for $\text{LET} \geq 80 \text{ MeV}\cdot\text{cm}^2/\text{mg}$ (or $80,000 \text{ MeV}\cdot\text{cm}^2/\text{g}$ in Fig. 19) is $1.5 \times 10^{-8} \text{ ions}\cdot\text{m}^{-2}\cdot\text{sr}^{-1}\cdot\text{s}^{-1}$. The SEDR rate (R) for an RTAX2000S device in this space environment is:

$$\begin{aligned} &= [4 \div 10^7 \text{ (ions}\cdot\text{cm}^{-2})] \times 2\pi \times 1.5 \times 10^{-8} \text{ (ions}\cdot\text{m}^{-2}\cdot\text{s}^{-1}) \\ &= 3.77 \times 10^{-18} \text{ s}^{-1} \\ &= 1.19 \times 10^{-10} \text{ yr}^{-1} \end{aligned}$$

So the mean time between SEDR events is approximately ten-billion years! Note that the majority, $\cong 99\%$, of antifuses are not in the critical path; and an antifuse rupture will most likely contribute only a few mA of leakage current.

Several comments about the calculation:

1. The test design is a typical case for SEDR events. The reasons are: the number of unused antifuses is independent of the design because about 95% of antifuses are not used for any design; and always about half of the unused antifuses are biased at V_{CCA} and the other half biased at GND.

2. Ions with $LET \geq \text{Threshold}$ cause SEDR at any incident angles. This causes an over estimate of the rate; in other words, this makes the estimate conservative.
3. Effective LET is not applicable. Ions with $LET < \text{Threshold}$ but at an angle other than normal incidence do not cause any SEDR because the normal incidence is the worst case.

Table I DUT parameters

Device	RTAX2000S
Package	CQ352
Foundry	UMC
Technology	0.15 μm CMOS
Die-Lot/Serial Number	D1L9R1: 73026 D1KHN1: 79023, 79102
Quantity Tested	3
IO Configuration	LVTTL
Design	SR_1000_4P_70_sp1

Table II Test Log

Run	DUT	Bias (V) V_{CC}/V_{CCA}	Temp ($^{\circ}\text{C}$)	Ion	LET $\text{MeV}\cdot\text{cm}^2/\text{mg}$	Tilt	Flux $\text{Ions}/\text{cm}^2/\text{s}$	Fluence Ions/cm^2	File Name	Comments
1	79023	3.7/1.7	125	Au	82.8	0	NA	NA	79023Au1	Run aborted
2	79023	3.7/1.7	125	Au	82.8	0	8.71E+04	9.97E+06	79023Au2	Functional
3	79023	3.3/1.5	125	Au	117.2	45	1.50E+05	9.97E+06	79023Au3	Functional
4	79023	3.6/1.65	125	Au	117.2	45	1.67E+05	1.00E+07	79023Au4	Functional
5	79023	3.3/1.5	125	Au	82.8	0	1.73E+05	1.00E+07	79023Au5	Functional
6	73026	3.3/1.5	125	Au	82.8	0	1.14E+05	9.99E+06	73026Au1	Functional
7	73026	3.6/1.65	125	Au	82.8	0	1.19E+05	9.96E+06	73026Au2	Functional
8	73026	3.3/1.5	125	Au	117.2	45	1.21E+05	9.96E+06	73026Au3	Functional
9	73026	3.6/1.65	125	Au	117.2	45	1.23E+05	1.00E+07	73026Au4	Functional
10	79102	3.3/1.5	125	Au	82.8	0	1.51E+05	1.00E+07	79102Au1	Functional
11	79102	3.6/1.65	125	Au	82.8	0	1.42E+05	9.98E+06	79102Au2	Functional
12	79102	3.3/1.5	125	Au	117.2	45	1.18E+05	1.00E+07	79102Au3	Functional
13	79102	3.6/1.65	125	Au	117.2	45	7.88E+04	9.99E+06	79102Au4	Functional
14	79102	3.6/1.65	125	Xe	69.8	45	1.12E+05	9.97E+06	79102Xe1	Functional
15	79102	3.6/1.65	125	Xe	49.3	0	1.12E+05	9.94E+06	79102Xe2	Functional
16	73026	3.6/1.65	125	Xe	49.3	0	1.11E+05	1.00E+07	73026Xe1	Functional
17	73026	3.6/1.65	125	Xe	69.8	45	1.04E+05	1.00E+07	73026Xe2	Functional
18	79023	3.6/1.65	125	Xe	49.3	0	1.05E+05	9.96E+06	79023Xe1	Functional
19	79023	3.6/1.65	125	Xe	69.8	45	1.12E+04	1.00E+07	79023Xe2	Functional

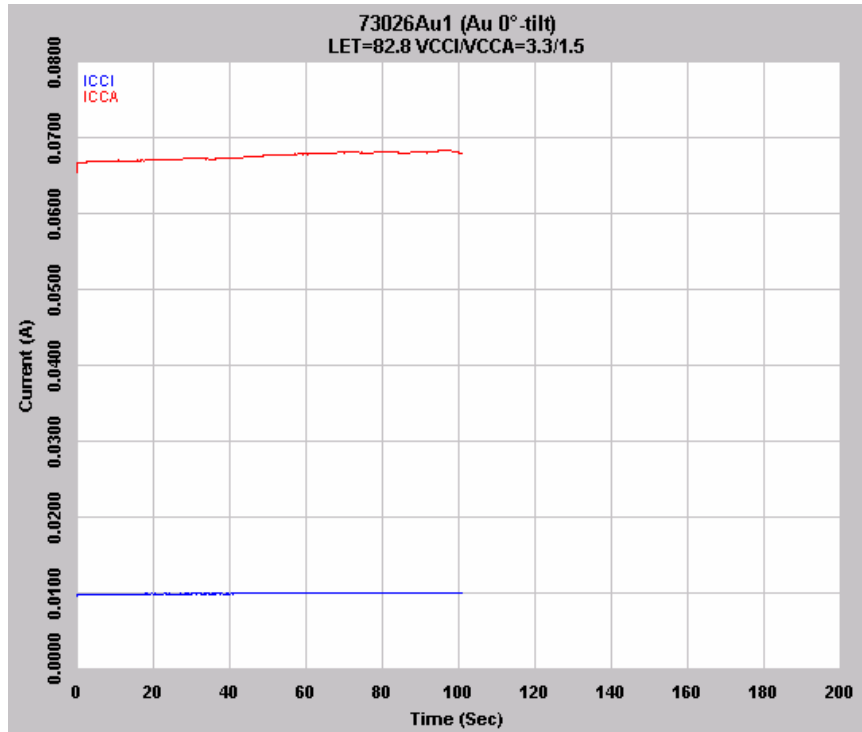


Fig. 1 Plot showing in-flux power supply currents (I_{CCI} and I_{CCA}) of DUT73026 irradiated by Au-ions with 0° tilt; effective LET = $82.8 \text{ MeV}\cdot\text{cm}^2/\text{mg}$; $V_{CCI}/V_{CCA} = 3.3 \text{ V}/1.5 \text{ V}$

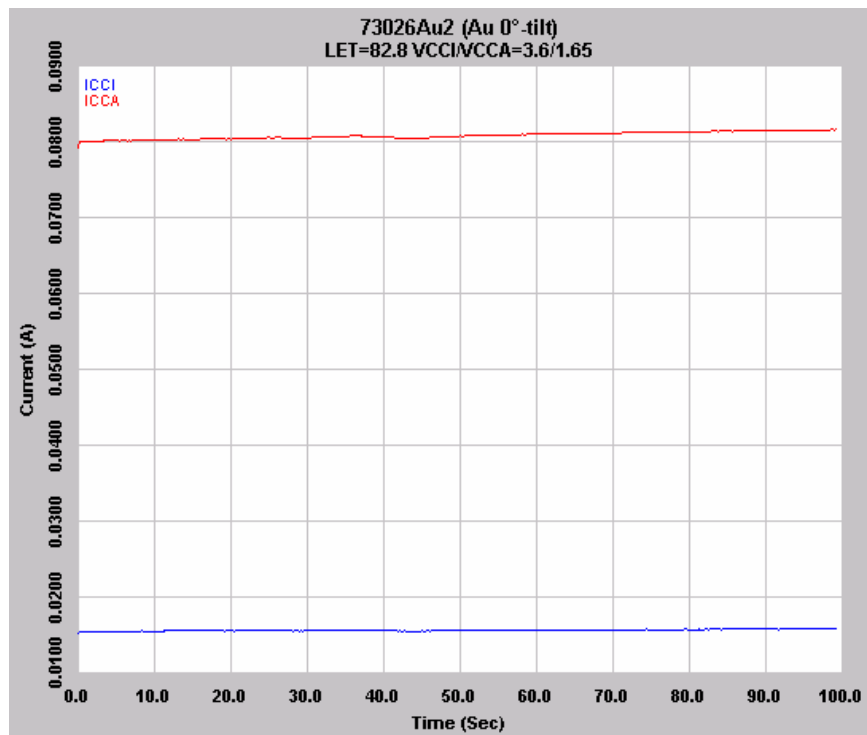


Fig. 2 Plot showing in-flux power supply currents (I_{CCI} and I_{CCA}) of DUT73026 irradiated by Au-ions with 0° tilt; effective LET = $82.8 \text{ MeV}\cdot\text{cm}^2/\text{mg}$; $V_{CCI}/V_{CCA} = 3.6 \text{ V}/1.65 \text{ V}$.

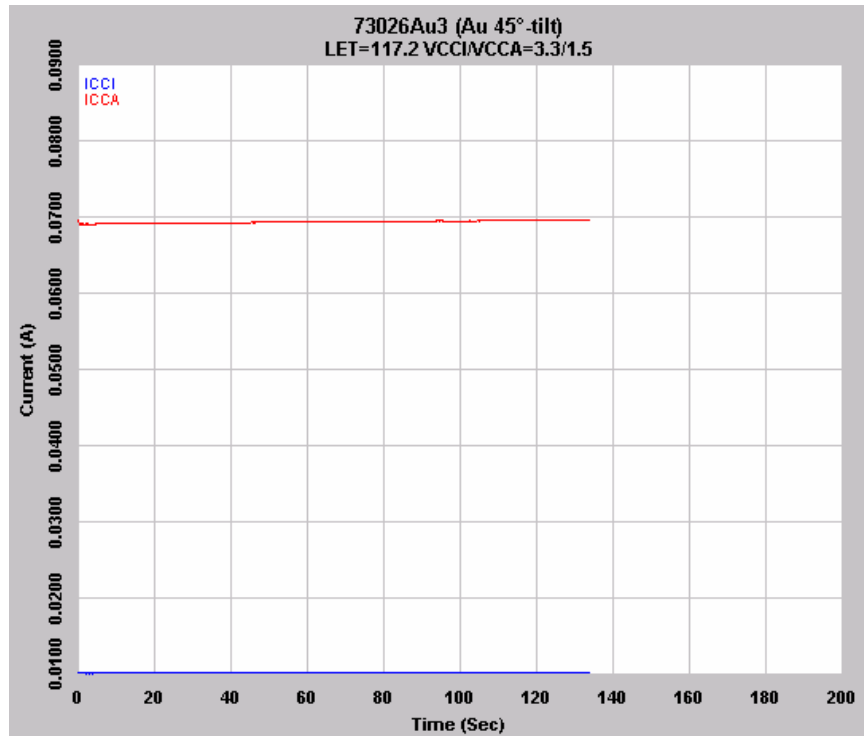


Fig. 3 Plot showing in-flux power supply currents (I_{CCI} and I_{CCA}) of DUT73026 irradiated by Au-ions with 45° tilt; effective LET = $117.2 \text{ MeV}\cdot\text{cm}^2/\text{mg}$; $V_{CCI}/V_{CCA} = 3.3 \text{ V}/1.5 \text{ V}$.

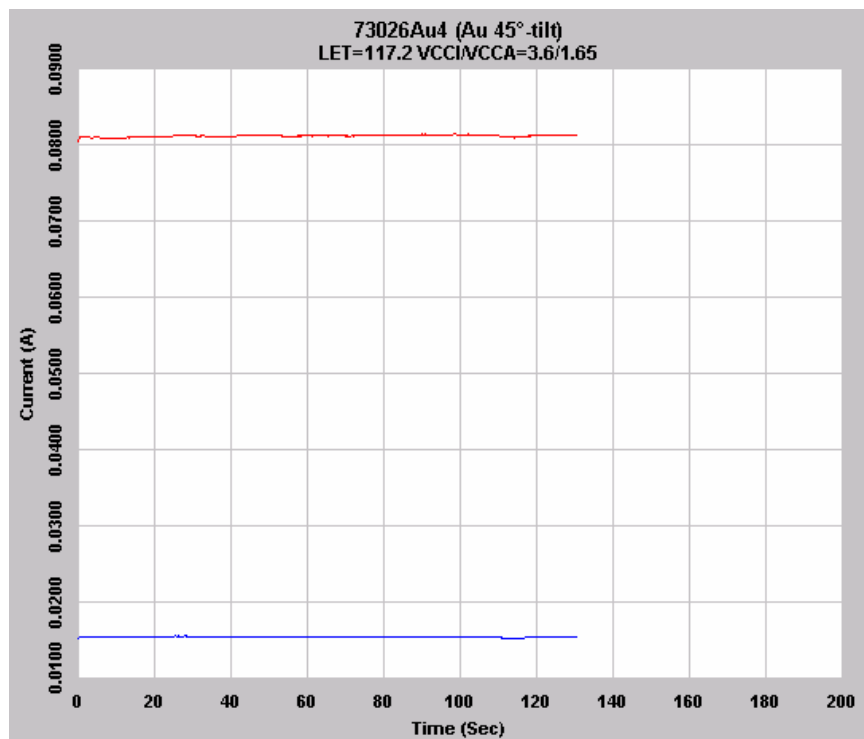


Fig. 4 Plot showing in-flux power supply currents (I_{CCI} and I_{CCA}) of DUT73026 irradiated by Au-ions with 45° tilt; effective LET = $117.2 \text{ MeV}\cdot\text{cm}^2/\text{mg}$; $V_{CCI}/V_{CCA} = 3.6 \text{ V}/1.65 \text{ V}$.

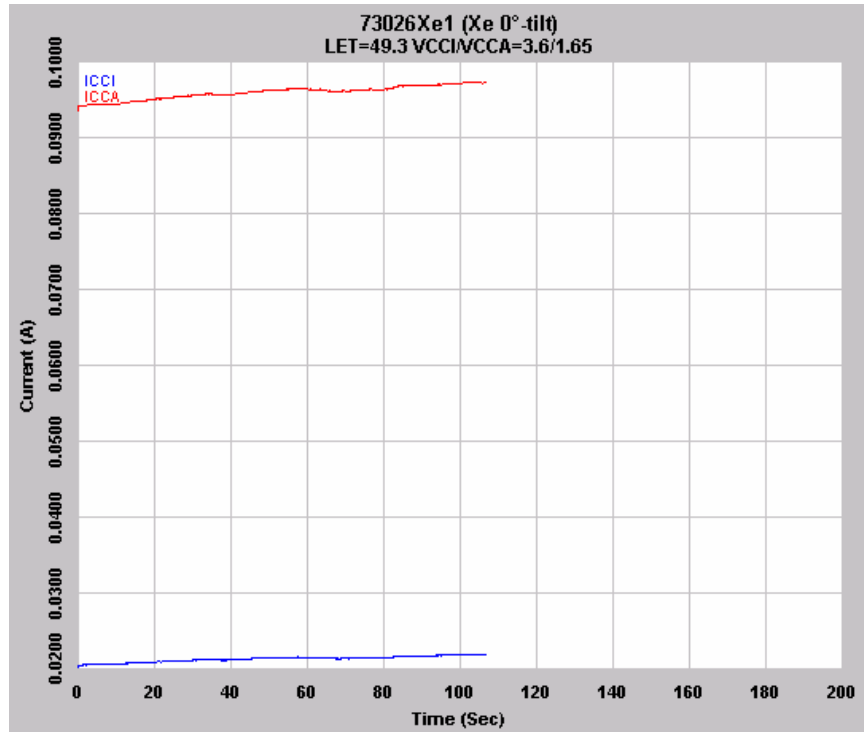


Fig. 5 Plot showing in-flux power supply currents (I_{CCI} and I_{CCA}) of DUT73026 irradiated by Xe-ions with 0° tilt; effective LET = $49.3 \text{ MeV}\cdot\text{cm}^2/\text{mg}$; $V_{CCI}/V_{CCA} = 3.6 \text{ V}/1.65 \text{ V}$.

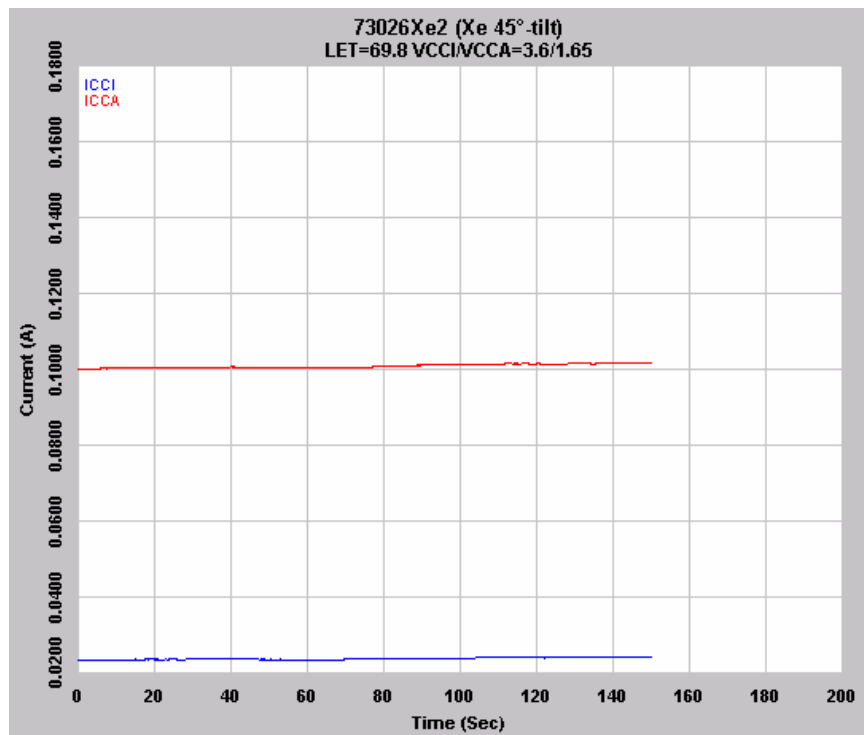


Fig. 6 Plot showing in-flux power supply currents (I_{CCI} and I_{CCA}) of DUT73026 irradiated by Xe-ions with 45° tilt; effective LET = $69.8 \text{ MeV}\cdot\text{cm}^2/\text{mg}$; $V_{CCI}/V_{CCA} = 3.6 \text{ V}/1.65 \text{ V}$.

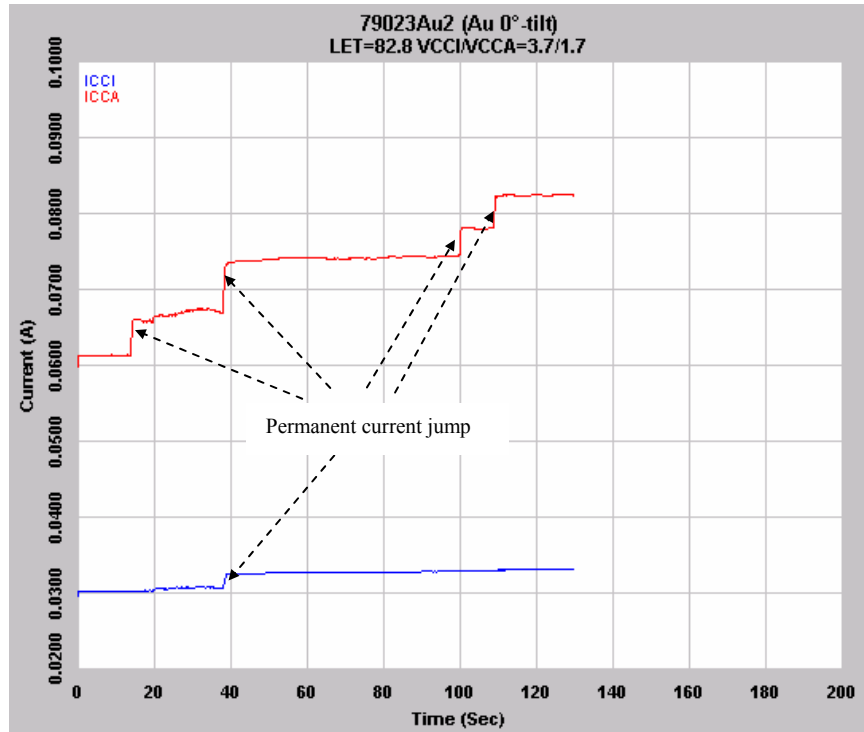


Fig. 7 Plot showing in-flux power supply currents (I_{CCI} and I_{CCA}) of DUT79023 irradiated by Au-ions with 0° tilt; effective LET = $82.8 \text{ MeV}\cdot\text{cm}^2/\text{mg}$; $V_{CCI}/V_{CCA} = 3.7 \text{ V}/1.7 \text{ V}$.

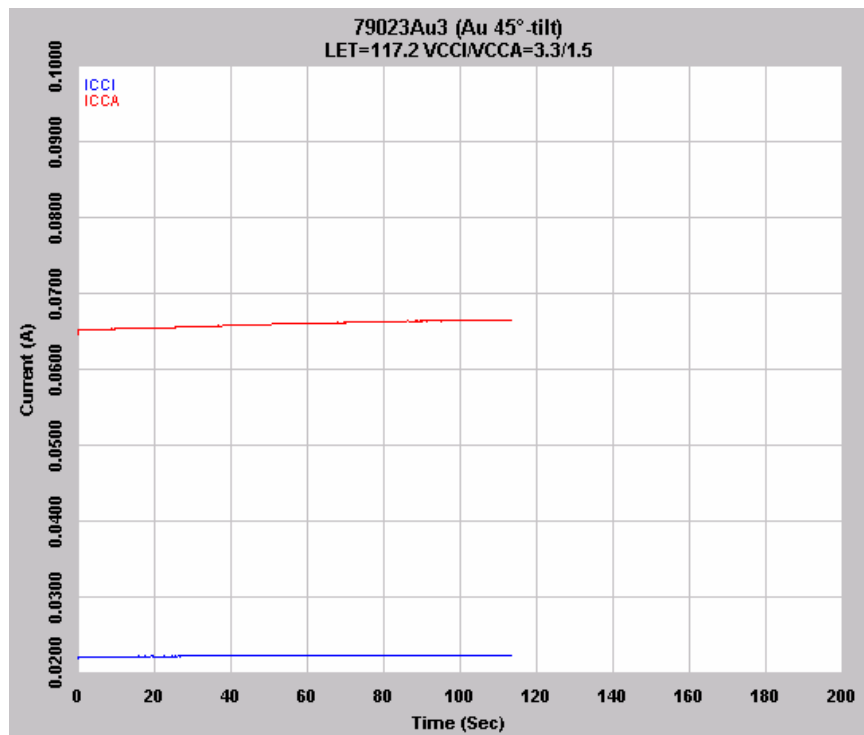


Fig. 8 Plot showing in-flux power supply currents (I_{CCI} and I_{CCA}) of DUT79023 irradiated by Au-ions with 45° tilt; effective LET = $117.2 \text{ MeV}\cdot\text{cm}^2/\text{mg}$; $V_{CCI}/V_{CCA} = 3.3 \text{ V}/1.5 \text{ V}$.

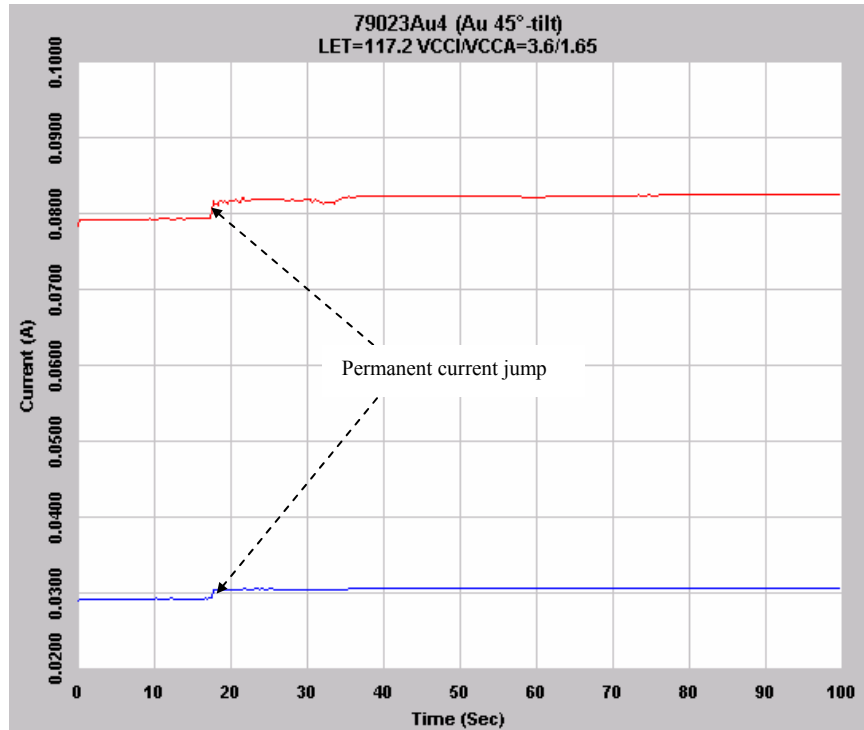


Fig. 9 Plot showing in-flux power supply currents (I_{CCI} and I_{CCA}) of DUT79023 irradiated by Au-ions with 45° tilt; effective LET = 117.2 MeV•cm²/mg; V_{CCI}/V_{CCA} = 3.6 V/1.65 V.

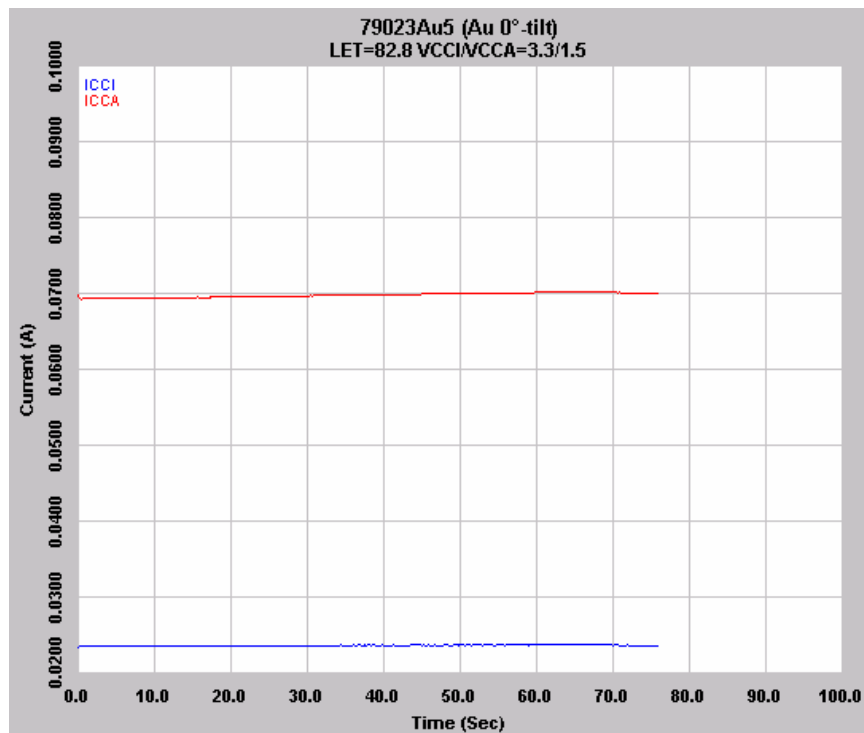


Fig. 10 Plot showing in-flux power supply currents (I_{CCI} and I_{CCA}) of DUT79023 irradiated by Au-ions with 0° tilt; effective LET = 82.8 MeV•cm²/mg; V_{CCI}/V_{CCA} = 3.3 V/1.5 V.

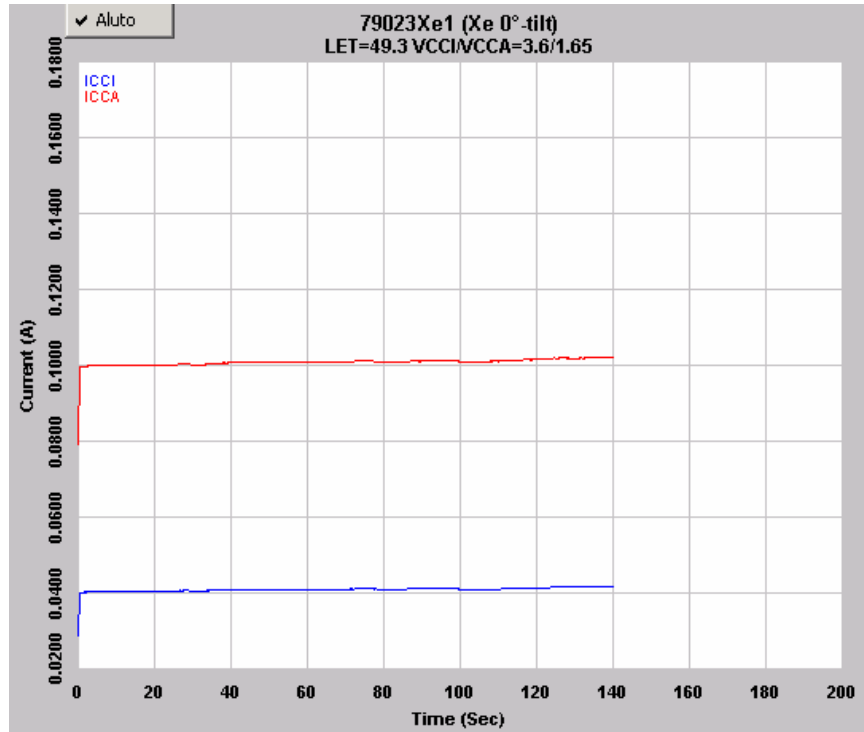


Fig. 11 Plot showing in-flux power supply currents (I_{CCI} and I_{CCA}) of DUT79023 irradiated by Xe-ions with 0° tilt; effective LET = $49.3 \text{ MeV}\cdot\text{cm}^2/\text{mg}$; $V_{CCI}/V_{CCA} = 3.6 \text{ V}/1.65 \text{ V}$.

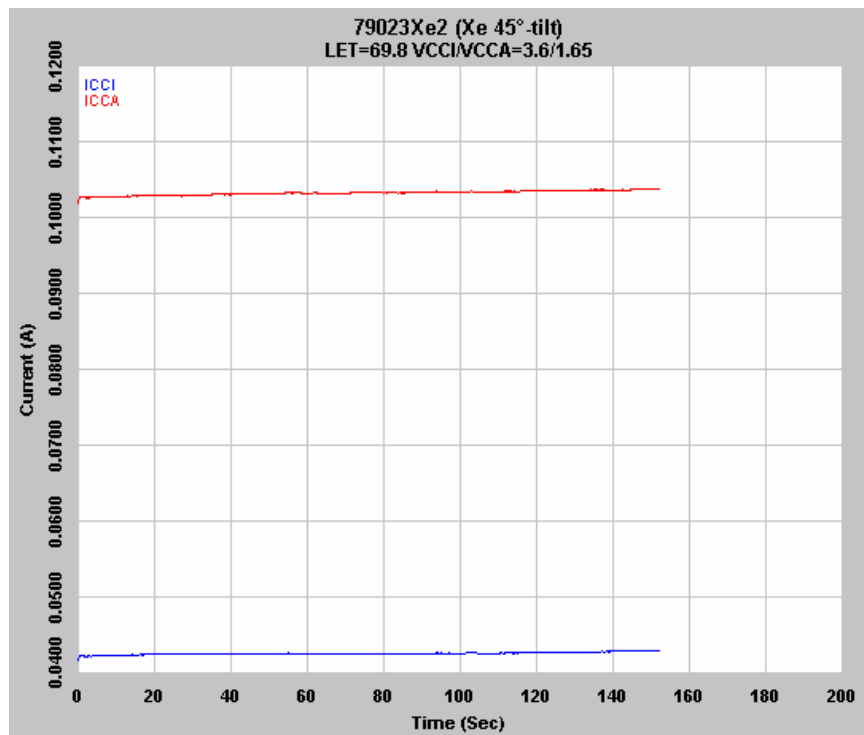


Fig. 12 Plot showing in-flux power supply currents (I_{CCI} and I_{CCA}) of DUT79023 irradiated by Xe-ions with 45° tilt; effective LET = $69.8 \text{ MeV}\cdot\text{cm}^2/\text{mg}$; $V_{CCI}/V_{CCA} = 3.6 \text{ V}/1.65 \text{ V}$.

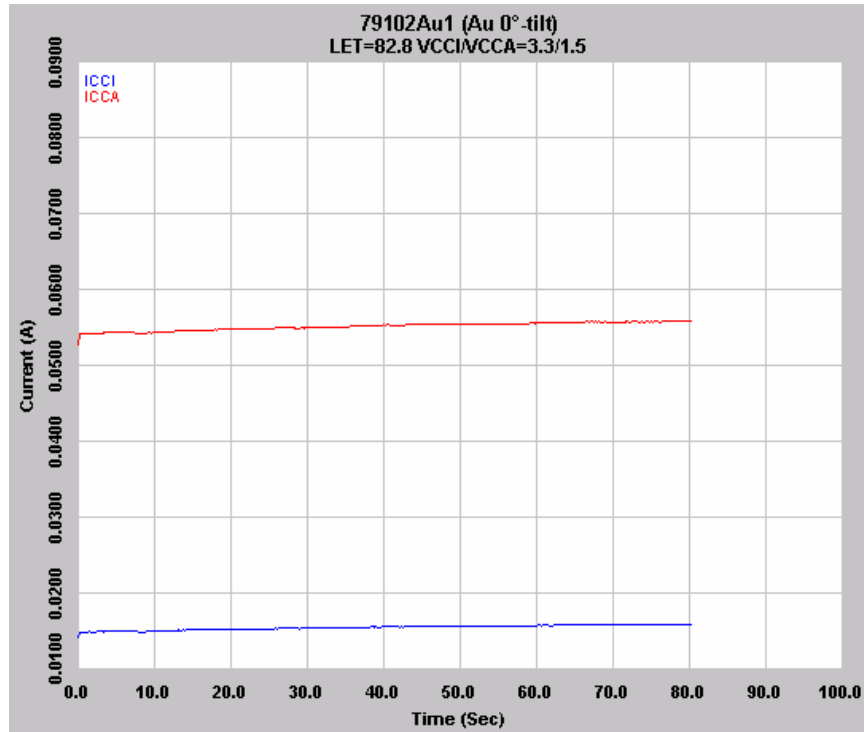


Fig. 13 Plot showing in-flux power supply currents (I_{CCI} and I_{CCA}) of DUT79102 irradiated by Au-ions with 0° tilt; effective LET = $82.8 \text{ MeV}\cdot\text{cm}^2/\text{mg}$; $V_{CCI}/V_{CCA} = 3.3 \text{ V}/1.5 \text{ V}$.

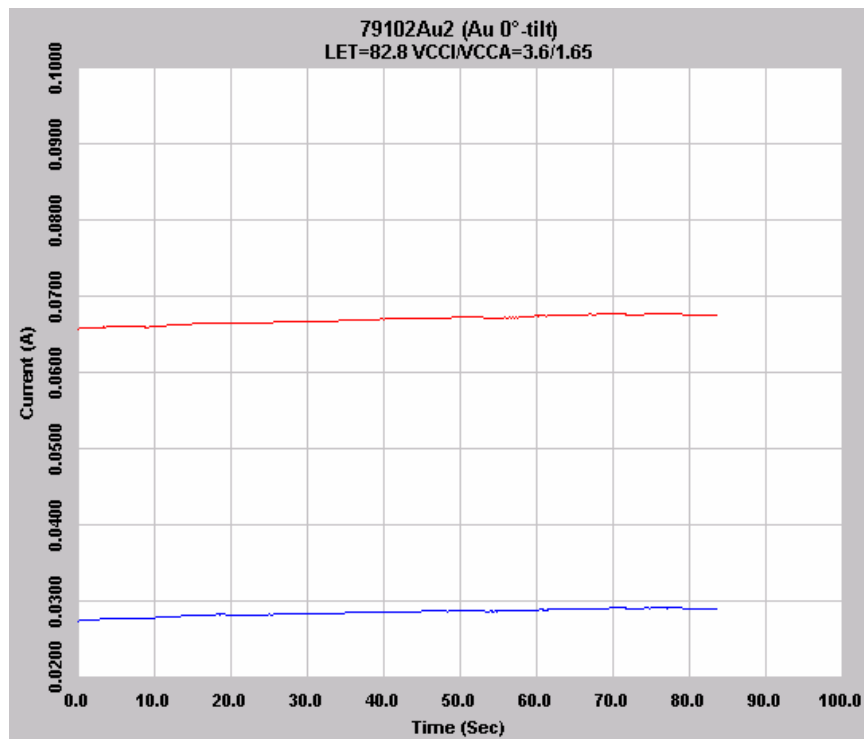


Fig. 14 Plot showing in-flux power supply currents (I_{CCI} and I_{CCA}) of DUT79102 irradiated by Au-ions with 0° tilt; effective LET = $82.8 \text{ MeV}\cdot\text{cm}^2/\text{mg}$; $V_{CCI}/V_{CCA} = 3.6 \text{ V}/1.65 \text{ V}$.

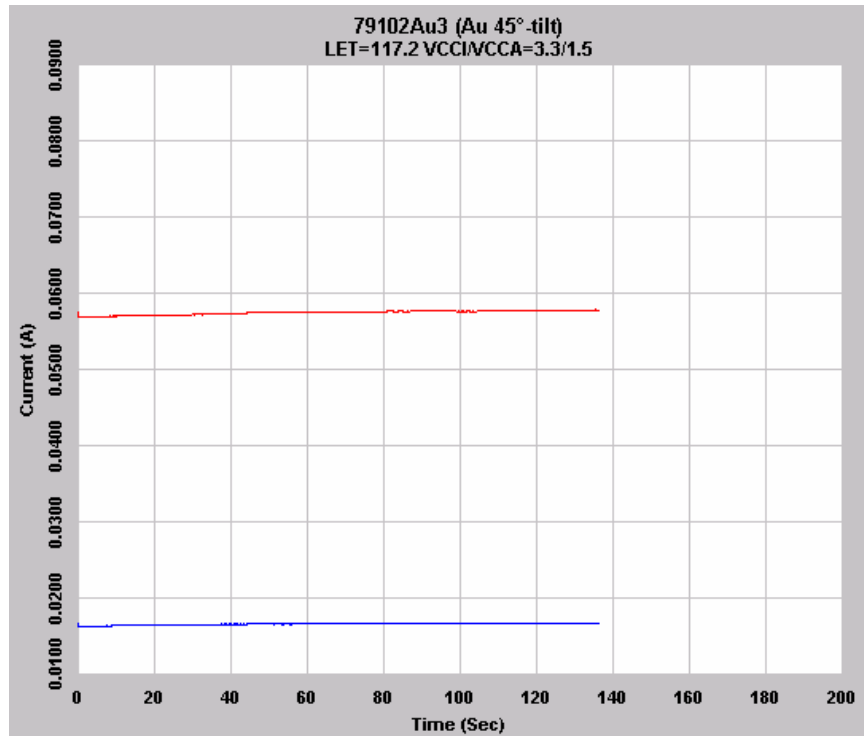


Fig. 15 Plot showing in-flux power supply currents (I_{CCI} and I_{CCA}) of DUT79102 irradiated by Au-ions with 45° tilt; effective LET = 117.2 MeV·cm²/mg; V_{CCI}/V_{CCA} = 3.3 V/1.5 V.

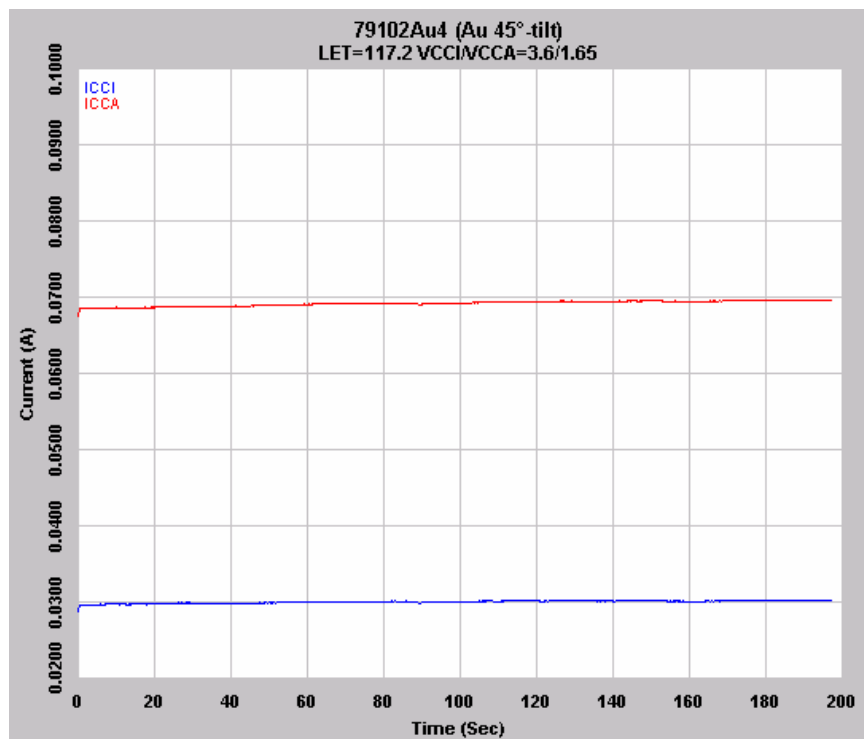


Fig. 16 Plot showing in-flux power supply currents (I_{CCI} and I_{CCA}) of DUT79102 irradiated by Au-ions with 45° tilt; effective LET = 117.2 MeV·cm²/mg; V_{CCI}/V_{CCA} = 3.6 V/1.65 V.

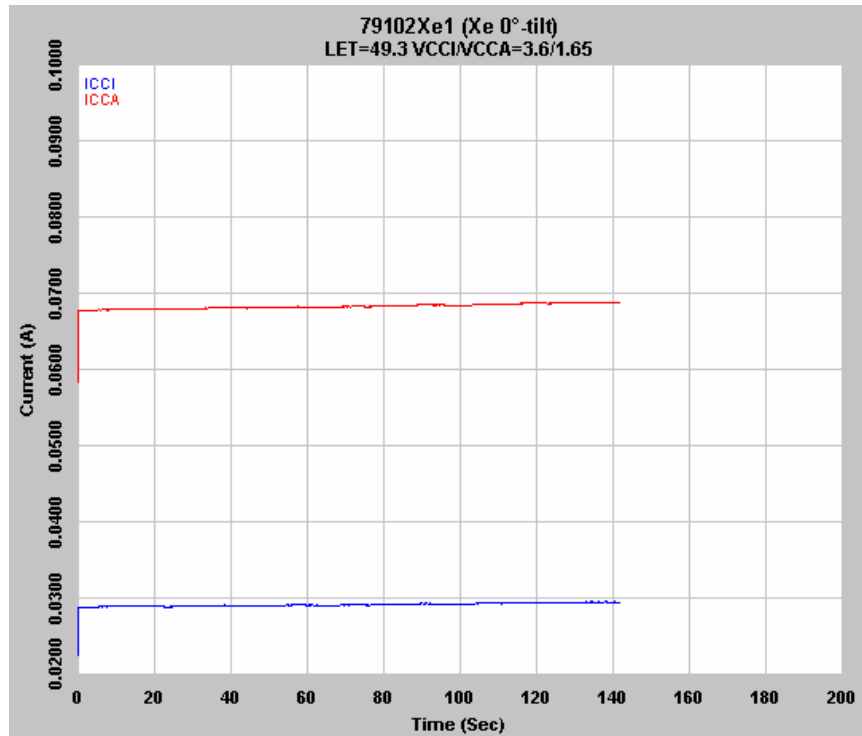


Fig. 17 Plot showing in-flux power supply currents (I_{CCI} and I_{CCA}) of DUT79102 irradiated by Xe-ions with 0° tilt; effective LET = $49.3 \text{ MeV}\cdot\text{cm}^2/\text{mg}$; $V_{CCI}/V_{CCA} = 3.6 \text{ V}/1.65 \text{ V}$.

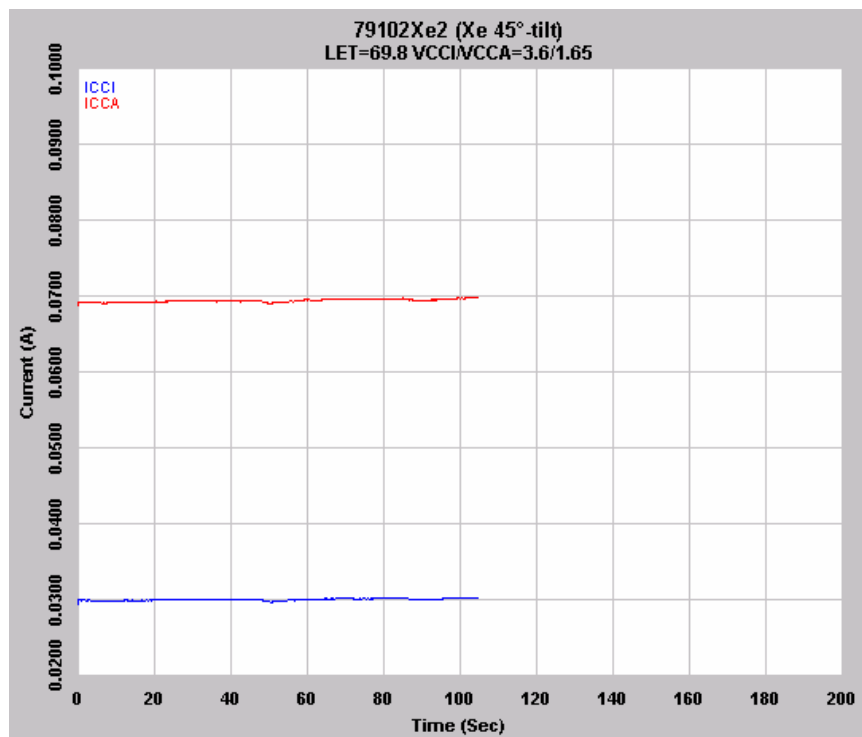


Fig. 18 Plot showing in-flux power supply currents (I_{CCI} and I_{CCA}) of DUT79102 irradiated by Xe-ions with 45° tilt; effective LET = $69.8 \text{ MeV}\cdot\text{cm}^2/\text{mg}$; $V_{CCI}/V_{CCA} = 3.6 \text{ V}/1.65 \text{ V}$.

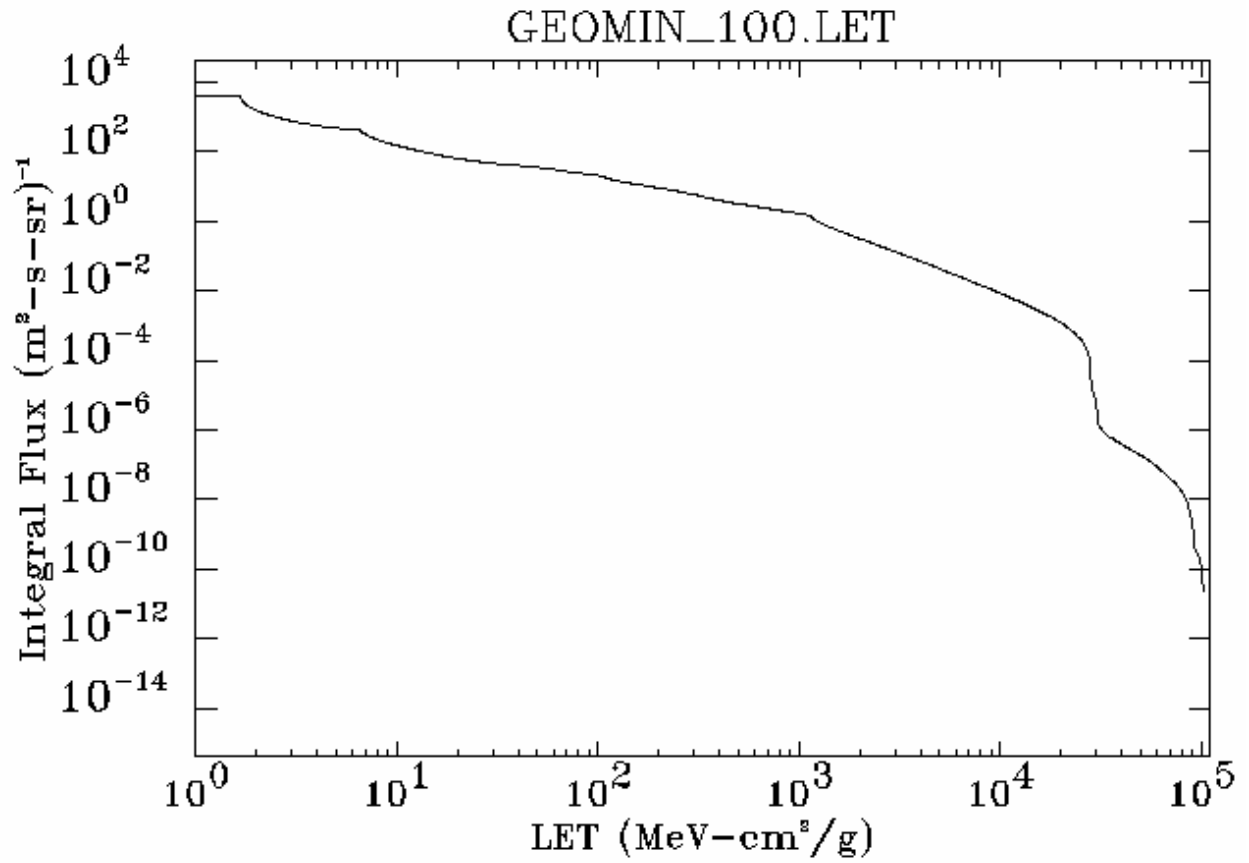


Fig. 19 Plot showing CRÈME96-generated integral flux versus LET in an environment of: geosynchronous orbit, solar minimum, and 100 mil Al shielding.