LX12973 VREF @ 800mV, 1.5A, 1.1MHz PWM



The LX12973 operates as a Current

Mode PWM Buck regulator that

switches to PFM mode with light

loads. The entire regulator function

is implemented with few external

The LX12973 responds quickly to

dynamic load changes using a high

internal compensation. Tight output

voltage regulation is maintained with

the compensated 800mV, +/-2%

reference (line and temp regulation).

With two external resistors the output

voltage is easily programmed, from

800mV to 90% of Vin.

bandwidth error amplifier

components.

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KEY FEATURES

- Internal Reference 800mv ±2% Accuracy (Line and Temp.)
- 4.5V to 5.5V Input Range
- Internal Soft Start
- Adj. Output From 0.8V to VIN
- Output Current (I >1.5A)
 Quiescent Current < 550uA, typ
- at 23°C
- 1.1MHz PWM Frequency
- Micro Lead-frame, Thin MO-229, 6-Pin Package

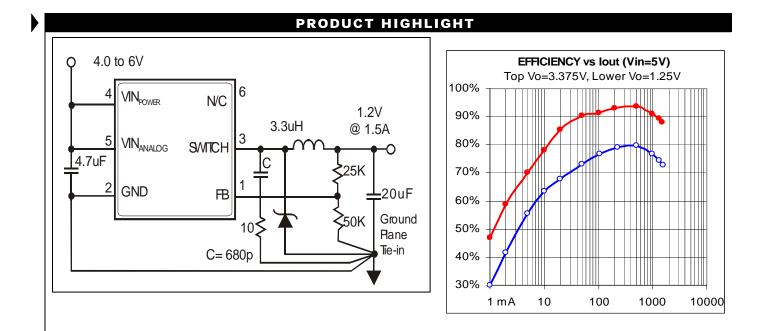
APPLICATIONS/BENEFITS

- Portable Microprocessor Core Voltage Supplies
- 5V to 3V
- RoHS compliant product

IMPORTANT: For the most current data, consult MICROSEMI's website: http://www.microsemi.com

DESCRIPTION

and



The regulator is capable of providing

an output load current of 1.5A, has no

minimum load current requirement for

cycle-by-cycle to protect the switch.

maximized with low low regulator IQ

The LX12973 operational range

covers 4.0V to 6.0V, features include

power on delay; soft start to limit

inrush currents; and thermal shutdown

The 6 pin MO-229 package provides

a small form factor with excellent

Current limit is

efficiency

is

stable operation.

Power conversion

during fault conditions.

power dissipation capability.

and PFM mode of operation

Figure 1 – LX12973 Circuit Topology and Typical Efficiency Performance

$T_{J}\left(^{o}C\right)$	Input Voltage	Output Voltage Range	Plastic MO2296 Pin (3mm²)RoHS Compliant / Pb-free	
0 to 125	4.5V – 5.5V	Adjustable	LX12973CLD	987 SC

Note: Available in Tape & Reel. Append the letters "TR" to the part number. (i.e. LX12973CLD-TR)

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FB

GND 2

SW 3

PACKAGE PIN OUT

6

5

4

LD PACKAGE (Top View) Note: Heatsink pad on bottom should be connected to ground or left floating.

N/C

MN ANALOG

MN PWR

Input Voltage (IN)	0.3V to 7.0V
SW to GND	$0.3V$ to $(V_{IN} + 0.3V)$
V _{FB} to GND	0.3V to +2V
SW Peak Current (Internally Limited)	1800mA
Operating Temperature Range	40°C to +125°C
Storage Temperature Range, T _A	65°C to 150°C
Maximum Junction Temperature	150°C
Package Peak Temp. for Solder Reflow (40 seconds max. exposure)	260°C (+0, -5)
Note: Exceeding these ratings could cause damage to the device. All voltages a	are with respect to
Ground. Currents are positive into, negative out of specified terminal.	

ABSOLUTE MAXIMUM RATINGS

THERMAL DATA: "LD" PACKAGE

THERMAL RESISTANCE-JUNCTION TO AMBIENT, θJA (Assumes NO AMBIENT AIRFLOW) 25-40°C/W (PCB layout dependent)

Junction Temperature Calculation: $T_J = T_A + (P_D \ge \theta_{JA})$. The θ_{JA} numbers are guidelines for the thermal performance of the device/pc-board system.

|--|

NAME	DESCRIPTION				
VIN ANALOG	Unregulated supply voltage input, ranging from +4V to 6.0V for internal analog control circuitry.				
VIN PWR	Unregulated supply voltage input (+4V to 6.0V), high current path, connects to PMOS Source of PWM switch.				
FB	Feedback input for setting programming output voltage.				
GND	Circuit ground providing bias for IC operation and high frequency gate drive bias, can be connected to heatsink terminal.				
SW	Inductor and commutation diode connection point. Connects to internal PMOSFET source.				

ELECTRICAL CHARACTERISTICS

	Parameter	Symbol	Test Conditions	Min	Тур	Max	Units
	Operating Range	V _{IN}	Functional operation guaranteed by design	4.5		5.5	V
	Feed Back Threshold	V _{FBT}	$4.0V \le V_{IN} \le 6.0V$	784	800	816	mV
	FB Input Current	I _{FB}	V _{FB} = 0.81V		40	75	nA
	Error Amplifier	BW	Closed Loop		100		Khz
	Quiescent Operating Current	I _Q (Pin 5)	V _{FB} > 0.825V, Rload Switch Pin < 1K ohms		500	850	μΑ
	Soft Start, Vout Slew Rate	Vo	Initial Power On or after Short Circuit		21	50	V/mS
	P-Channel Switch ON Resistance	R _{DS(ON)}	I _{SW} = 1.0A		0.25	0.5	Ω
	Maximum Duty Cycle	D	$I_{SW} = 1.0A$ (assured by design, not ATE tested)	80	100		%
	SW Leakage Current	I _{LEAK}	V _{FB} = 0.825V		0.01	5	μΑ
	P-Channel Current Limit	I _{LIM}	Peak Current at Switch Pin (not dc current)	1.6	1.9		А
	PWM Frequency	F _{OP-PWM}	PWM Mode	700	1020	1400	KHz
	PFM Mode Region	lo	PFM Mode		250		mA
	Feed Back PSRR		1hz < Frequency Vin < 10Khz		-40		dB
	Closed Loop Load Regulation	Load Reg	$V_{\rm O}$ = 1.2V, 50mA \leq I _O \leq 1.2A, ckt figure 1		0.85		%Vo
	Thermal Shutdown	T _{SD}	(assured by design, not ATE tested)	135	150		°C

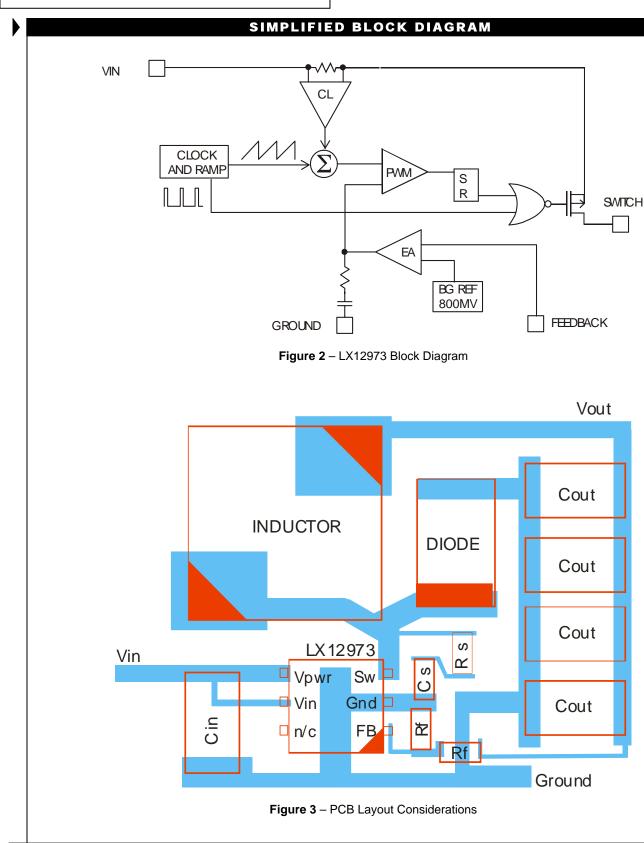
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APPLICATION NOTE

FUNCTIONAL DESCRIPTION

The LX12973 is a Current Mode PWM regulator with internal compensation.

The internal PMOS high side switch is protected with current limit on a pulse by pulse basis and with thermal shutdown. Thermal shutdown is activated with a junction temperature of 160°C (typical) and has 20°C of hysteresis.

The regulator has an internal Power On Reset delay of 50-100us to ensure all circuitry is operating before enabling the Switch output.

Soft Start is activated upon initial power-on, or following recovery from either thermal shutdown or short circuit. The Soft start control block generates a voltage ramp that clamps the error amplifier non-inverting reference voltage. As this clamp voltage rises, the duty cycle is gradually increased, thus limiting the peak inrush currents.

PWM / PFM mode of operation is determined by the load current condition. The PFM mode increases system efficiency by reducing the switching frequency thus switching losses. During light loading, Iout < 200ma typically, PFM mode becomes active, the switching frequency begins to decrease, the frequency change occurs over a continuous range, decreasing further as Iout decreases.

OUTPUT VOLTAGE PROGRAMMING

Resistors R1 and R2 program the output voltage. The value of R2 (lower resistor of divider) should be less than $10K\Omega$. The value of R1 can be determined using the following equation, note V_{REF} is also referred to as V_{FBT}.

$$R1 = R2 \left[\left(\frac{V_{OUT}}{V_{REF}} \right) - 1 \right]$$

DIODE SELECTION

A Schottky diode is required for switching speed and low forward voltage. Efficiency is determined mostly by the diode's forward voltage. The diode conducts 1-D%, for Vout=1.2V this becomes 76% in a 5V system.

INDUCTOR SELECTION

Selecting the appropriate inductor type and value ensures optimal performance of the converter circuit for the intended application. A primary consideration requires the selection of an inductor that will not saturate at the peak current level. EMI, output voltage ripple, and overall circuit efficiency affect inductor choice. The inductor that works best depends upon the application's requirements and some experimentation with actual devices in-circuit is typically necessary to make the most effective choice.

INDUCTOR SELECTION, CONT.

The LX12973 allows for a broad selection of inductor values and choosing a value between 2.2μ H and 22μ H supports a majority of applications. The benefit of a larger inductor value can increase efficiency at the lower output currents and reduces output voltage ripple, thus output capacitance related to ripple filtering. Smaller inductors typically provide smaller package size (critical in many portable applications) at the expense of increasing output ripple current. Regardless of inductor value, selecting a device manufactured with a ferrite-core produces lower losses at higher switching frequencies and thus better overall performance. Larger inductors may lead to diminished Step-Load response.

CAPACITOR SELECTION

To minimize ripple voltage, output capacitors with a low series resistance (ESR) are recommended. Multi-layer ceramic capacitors with X5R or X7R dielectric make an effective choice because they feature small size, very low ESR, a temperature stable dielectric, and can be connected in parallel to increase capacitance. Typical output capacitance values of 10 to 30μ F has proven effective. Other low ESR capacitors such as solid tantalum, specialty polymer, or organic semiconductor, make effective choices provided that the capacitor is properly rated for the output voltage and ripple current. Finally, choose an input capacitor of sufficient size to effectively decouple the input voltage source impedance (e.g., $C_{IN} \ge 4.7\mu$ F).

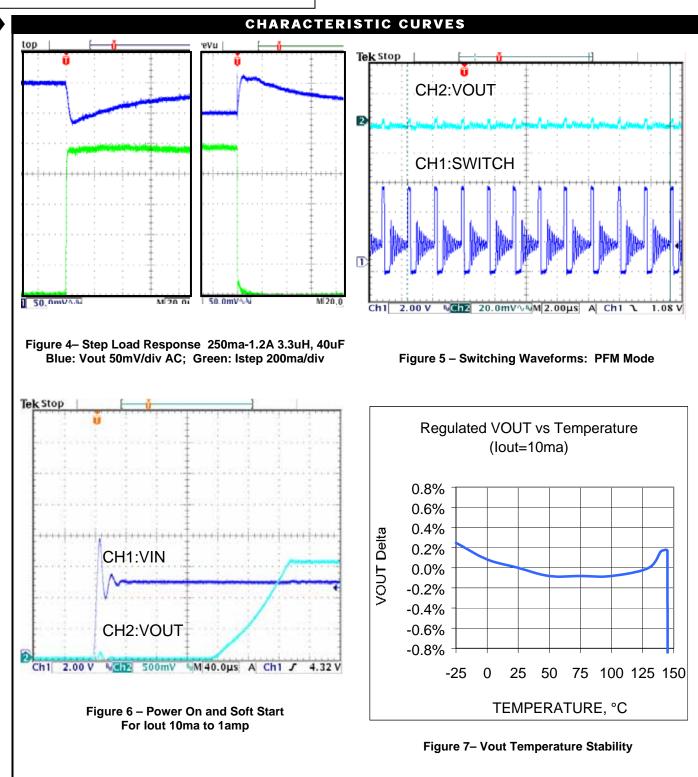
LAYOUT CONSIDERATIONS

The high peak currents and switching frequencies present in DC/DC converter applications require careful attention to device layout for optimal performance. Basic design rules include: (1) maintaining wide traces for power components (e.g., width > 50mils); (2) place C_{IN} , C_{OUT} , the Schottky diode, and the inductor close to the LX12973; (3) minimizing trace capacitance by reducing the etch area connecting the SW pin to the inductor; and (4) minimizing the etch length to the FB pin to reduce noise coupling into this high impedance sense input. Other considerations include placing a 0.1uF capacitor between the LX12973 VOUT pin and GND pin to reduce high frequency noise and decoupling the VIN pin using a 0.1uF capacitor. The LX12973 Switch has fast switching speeds which may generate noise spikes when a high capacitance Schottky diode is selected for the catch diode. A simple snubber circuit, as shown in Figure 1, R=10 ohms and C=680pF has proven effective to reduce the spike voltage generated at the Switch Pin / Diode connection.



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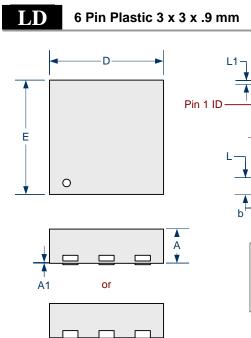


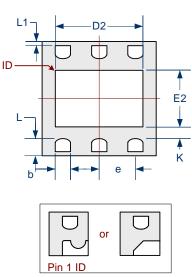
GRAPHS



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PACKAGE DIMENSIONS

	MILLIN	IETERS	INCHES				
Dim	MIN	MAX	MIN	MAX			
А	0.80	1.00	0.031	0.039			
A1	0.00	0.05	0.000	0.002			
Κ	0.20 MIN		0.008 MIN				
е	0.95 BSC		0.037 BSC				
L	0.30	0.50	0.012	0.02			
b	0.30	0.45	0.012	0.018			
D2	1.90	2.40	0.75	0.094			
E2	1.15	1.65	0.045	0.065			
D	3.00 BSC		0.118 BSC				
Е	3.00 BSC		0.118 BSC				
L1	0.00	0.15	0.000	0.006			

Note:

1. Dimensions do not include mold flash or protrusions; these shall not exceed 0.155mm(.006") on any side. Lead dimension shall not include solder coverage.

NOTES

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